

Kornilov, I. I. The conversion rate of magnesium-cadmium alloys into solid solutions. Moskva, Izd-vo Akademii nauk SSSR, 1935.

53 p. Cyr. 4 TN 26

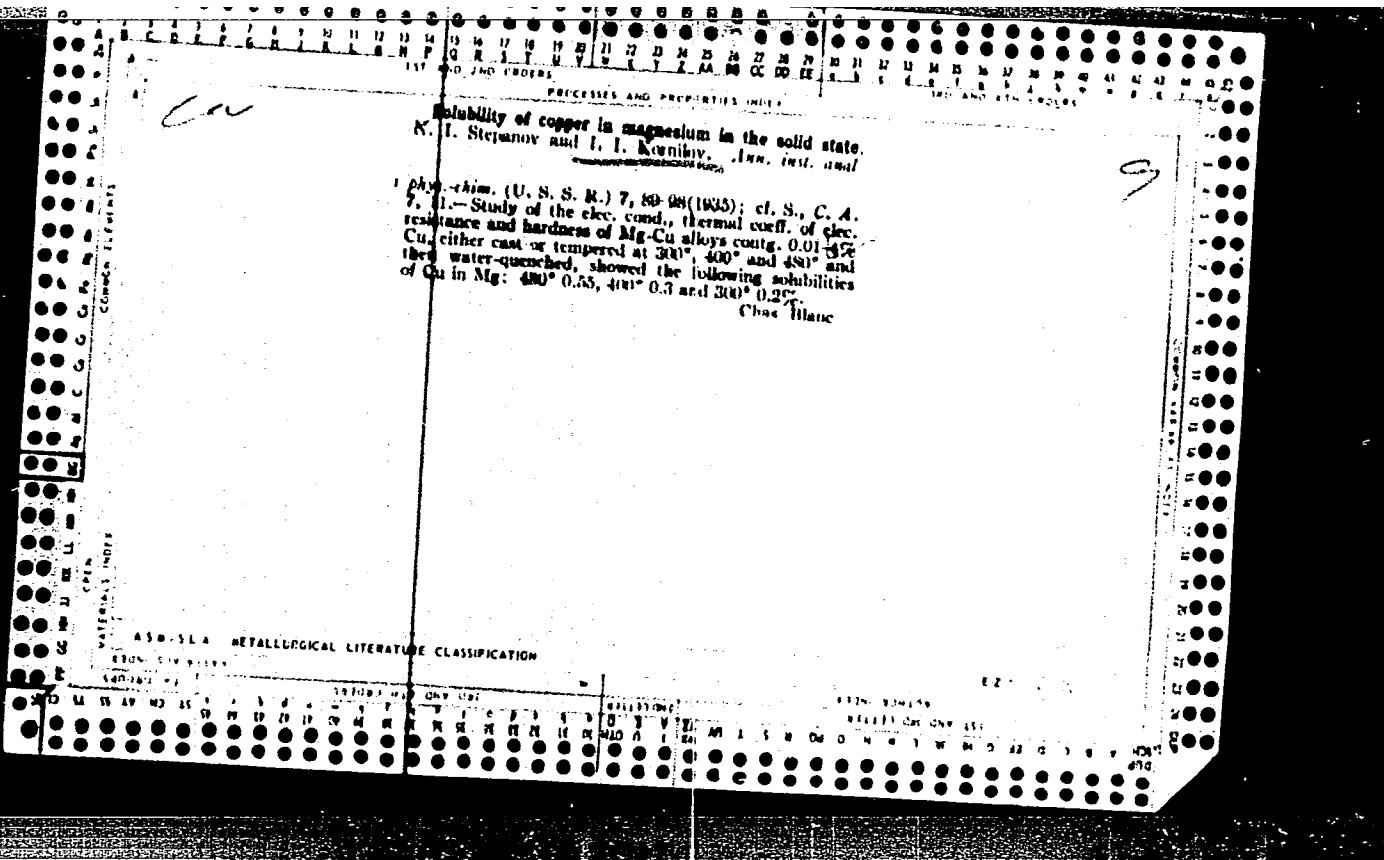
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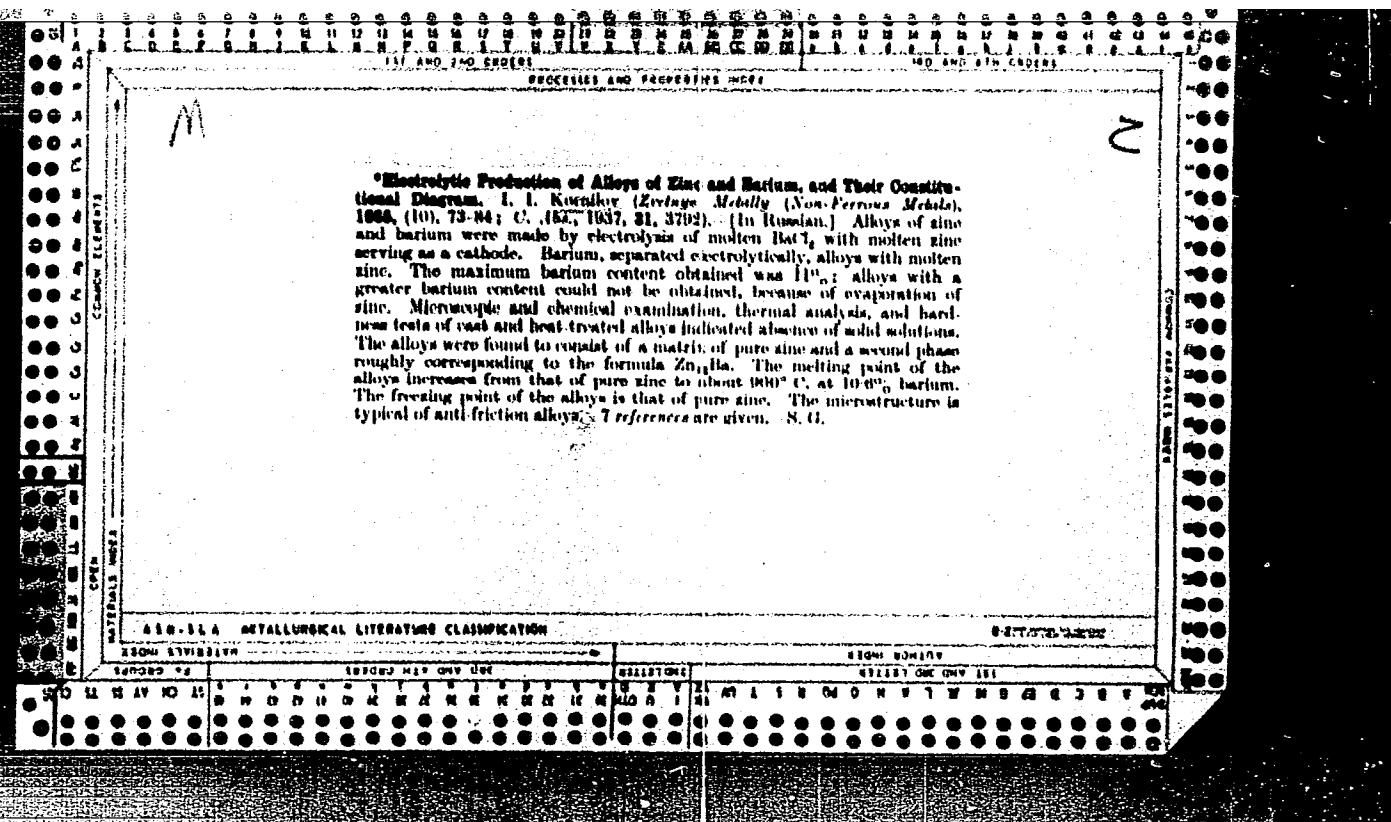
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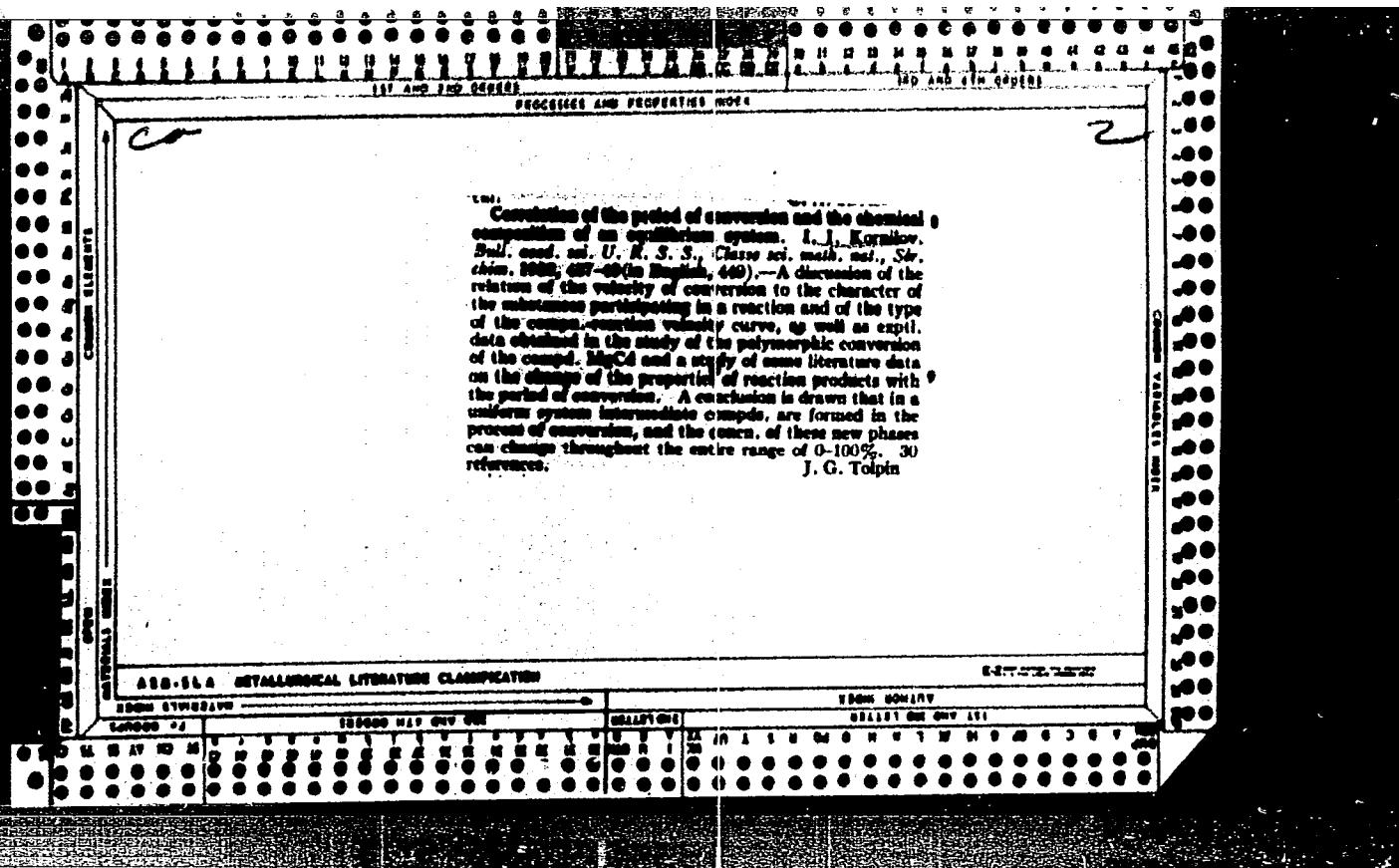
Velocity of polymorphic transformation of the compound $\beta\text{-MgO}_2$ in the system magnesium-oxides. I. I. Kostyuk (Bull. Acad. Sci. U.R.S.S., 1957, 313-337). Martens, conductivity, and microstructural changes indicate that the transition point of α_1 to $\beta\text{-MgO}_2$ is at 318°. The hardness of the alloys increases to a max. during the formation, owing to internal stresses involved in the rearrangement.

R. T.

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION







(1) *2000* *100* *CROSS*

PROCESSES AND PROPERTIES OF...

The fusion diagram of magnesium-cadmium alloys.

N. I. Stepanov and I. I. Kornikov, *Ann. secteur anal. phys.-chim., Inst. chim. (U. S. S. R.)* 10, 67-77 (1938).—In the thermal investigation of Mg-Cd alloys the danger of oxidizing the melt and overcooling during cryst. was overcome by working in a closed system in a H₂ atm. and mixing the melt in a closed Fe crucible by vertical rocking. An Fe tube, closed at the top and provided with a Pt-Pt-Rh thermocouple, was welded into the crucible bottom. Mixing, varying in at. % of Mg (sublimed) from 25 to 60%, were heated to 700° and then allowed to cool. The diagram consists of 2 branches intersecting at the point corresponding to the compd. MgCd, cryst. at a definite temp. (420°). The cryst. temp. is affected by the purity of metals used. Only the melt with 50% Mg showed a definite max.; this disproves the formation of MgCd₂ during crystn., which according to Hume-Rothery and Rowell (*C. A.* 21, 3328), is formed by the peritectic reaction of the Mg-Cd melt. The absence of MgCd₂ and the transition of MgCd from the α to δ cryst. modification at 250° was confirmed by microscopic exam. of the annealed melts (cf. Crubé, *Z. anorg. Chem.* 40, 72 (1900)). The velocity of transition in magnesium-cadmium alloys in the region of the compound MgCd. *Ibid.* 78-95; cf. *C. A.* 30, 2807.—The velocity of chem. transition of solid solns. of Mg-Cd, varying in at. percentage of Mg from 72 to 78%, was studied by the previous method of measuring the elec. cond. at various temps. A max. in the curve at 75 at. % Mg proves that MgCd has the max. rate of transition. The change in the structure of annealed solid solns. during the transi-

tion to a chem. compd. was studied by alternate heating at 100° and rapid cooling with H₂O. A series of photomicrographs shows that in the course of gradual transition the polyhedral microstructure of the solid soln. becomes increasingly cleaved; this indicates that the formation of MgCd is accompanied by a considerable vol. contrac-
tion. Approx. 25 references. The velocity of transition in magnesium-cadmium alloys in the region of the compound MgCd. *Ibid.* 97-112. In the similar study of Mg-Cd alloys with 20.8 at. % Mg, the curve shows a max. at 25 at. % Mg; this indicates that MgCd has the max. rate of transition. A similar change in the crystal structure during the chem. transition to MgCd took place.

Chav. Blanche

ASM-1A METALLURGICAL LITERATURE CLASSIFICATION

SECTION DIVISION

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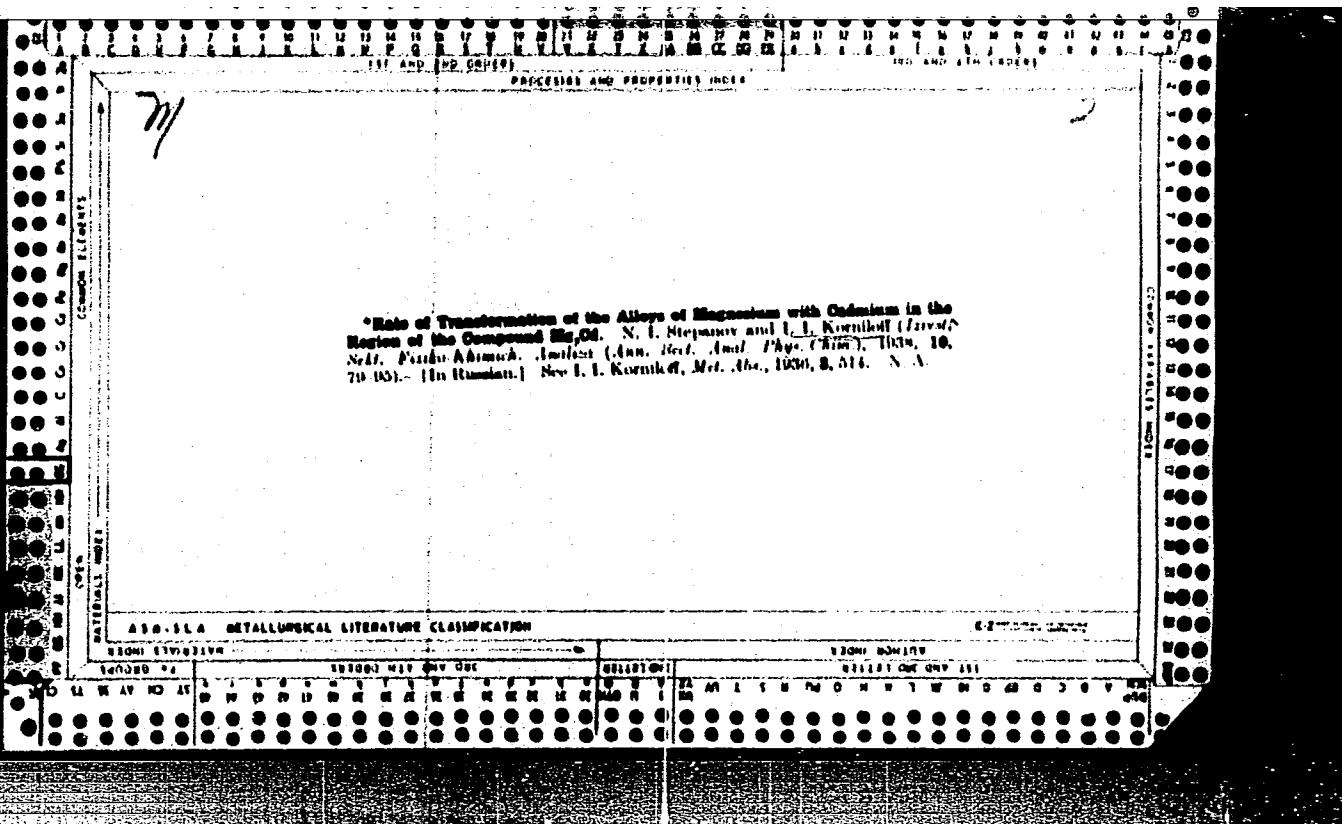
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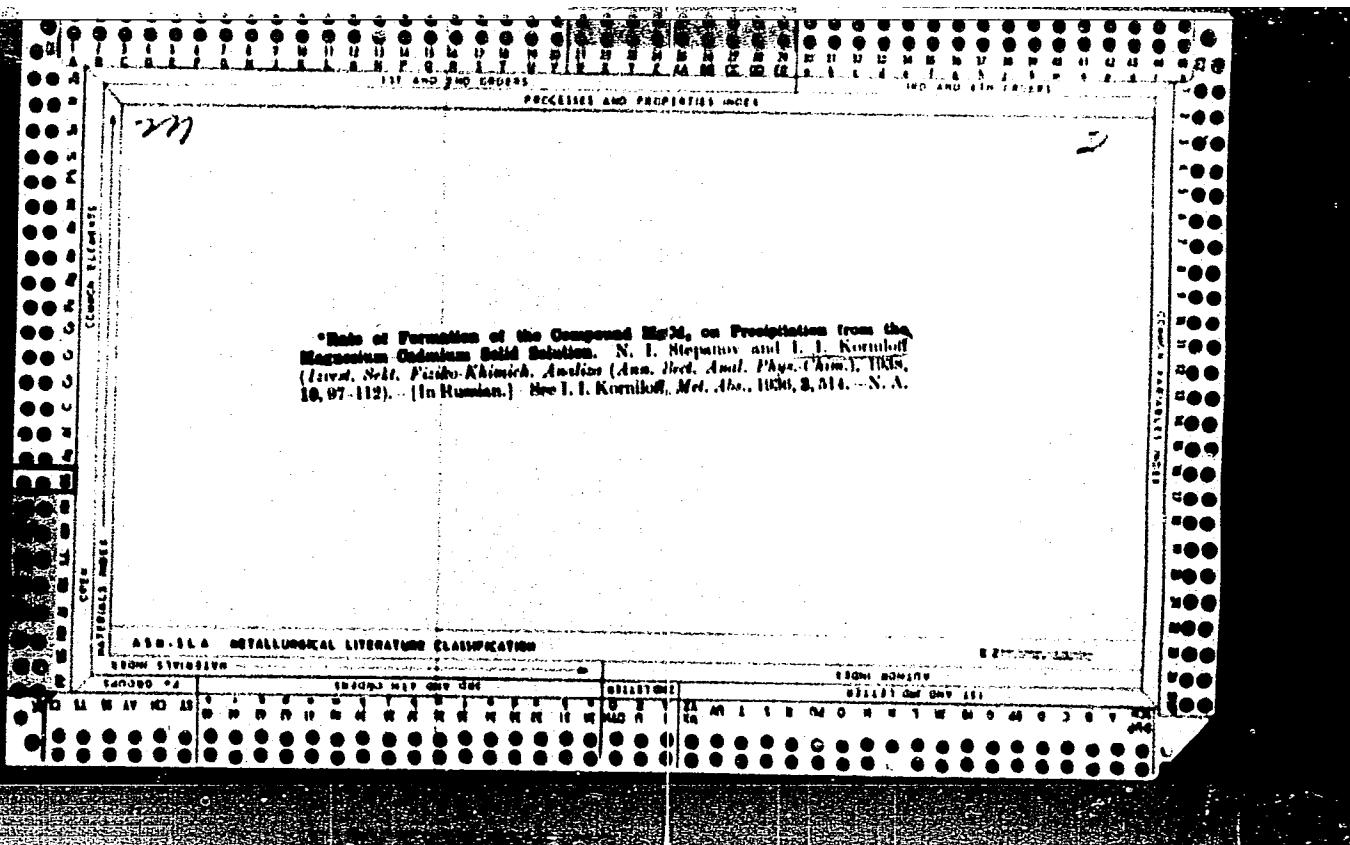
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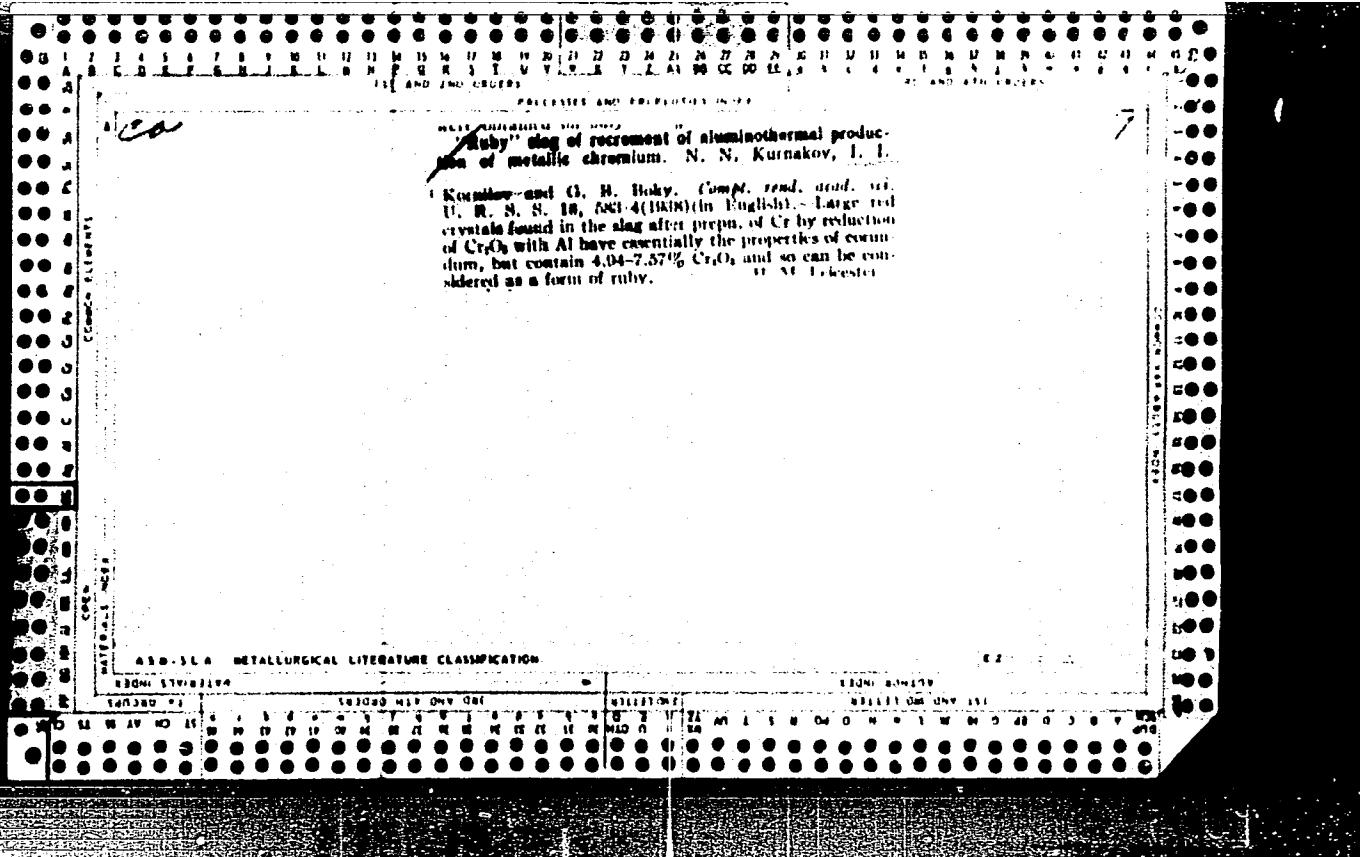
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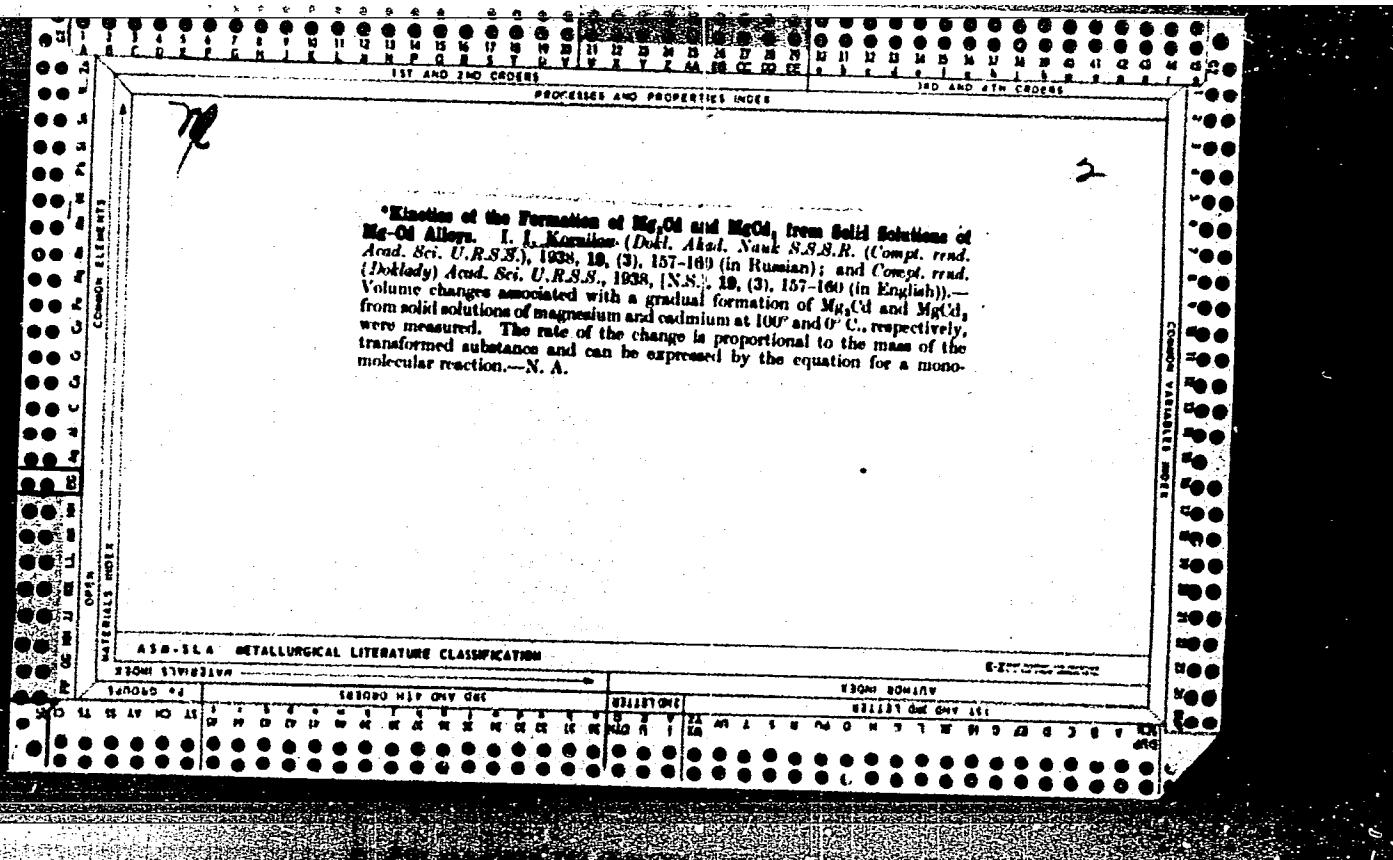
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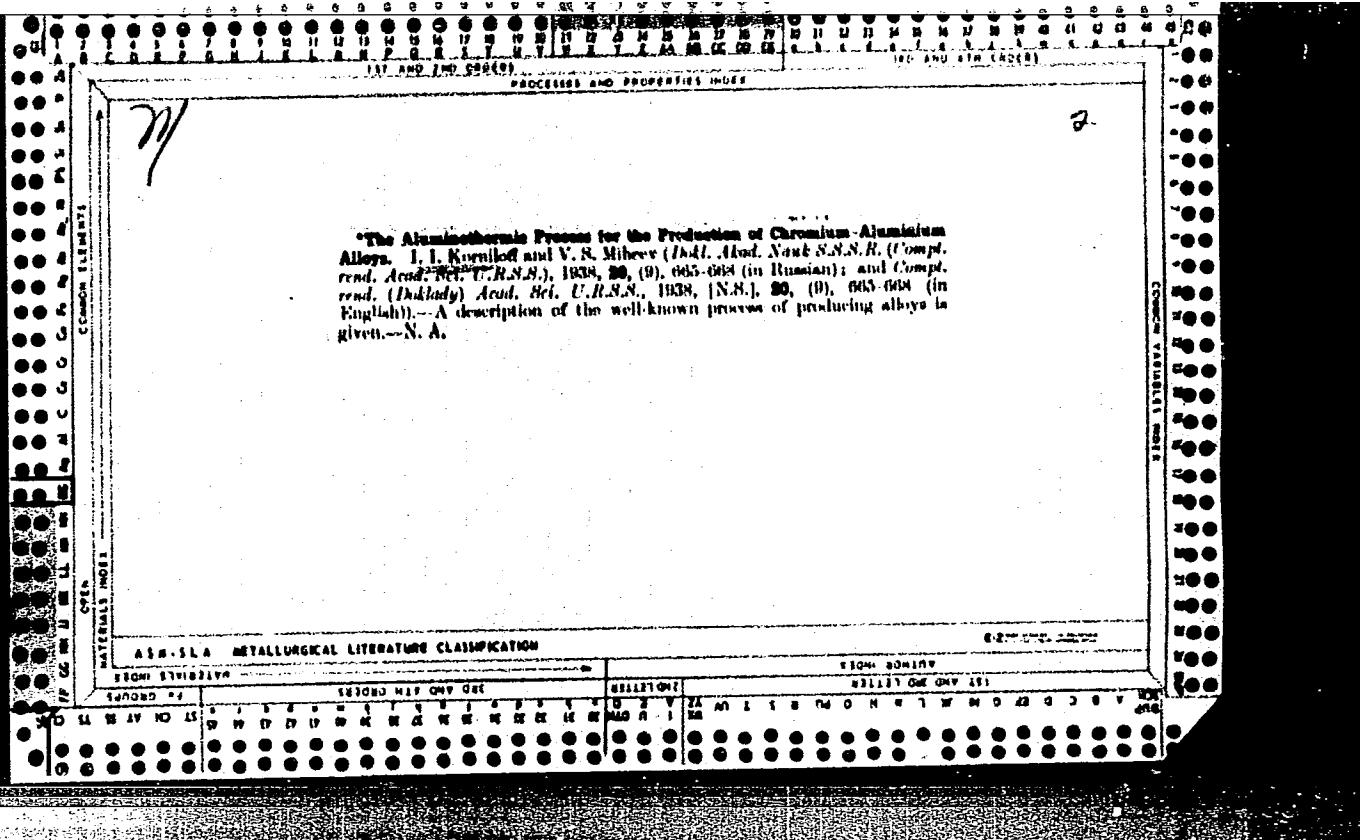
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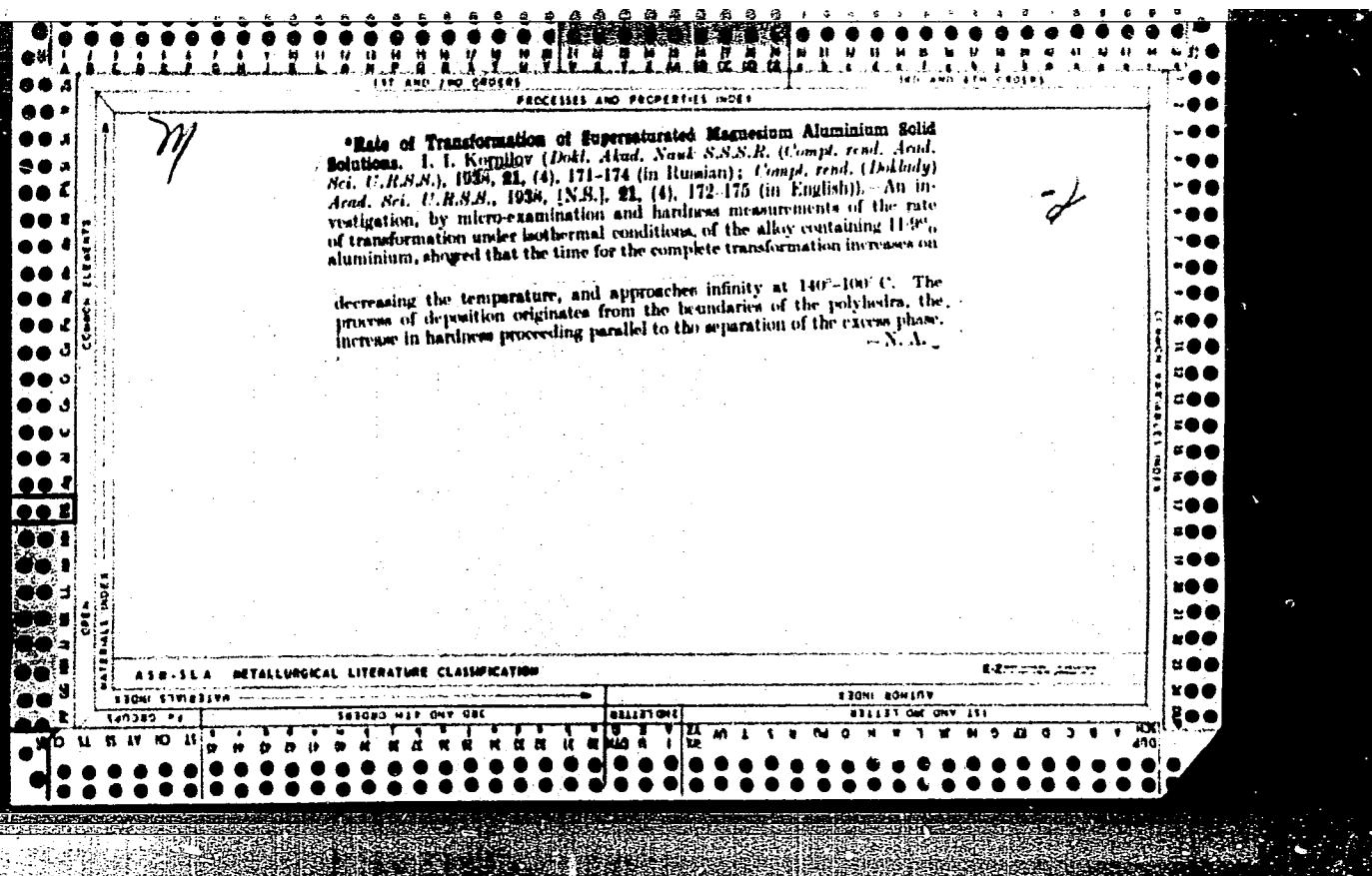












Conversion velocity of supersaturated solid solutions of magnesium-aluminum. I. I. Kornilov. *Compt. rend.*, Acad. Sc. U. R. S. S. 21, 172-5 (1939) (in English).—Investigations of excess phase pptn. with supersatd. solid solns. of Mg-Al alloys (11.9% Al) at 350, 300, 250, 150 and 100° led to the establishment of the full conversion time and its relation to temp., in the form of a curve the zero value of which corresponds to the min. point (425°) of a solid soln. on the solv. curve. The conversion time curve with increasing temp. goes off into infinity at about 140-100°, this being the interval of the unstable, tempered condition of alloys. The change in microstructure showed that the conversion process is heterogeneous. The hardness changes in accordance with the change in microstructure. During isothermal conversions in the interval of usual aging temps. the hardness rises parallel with the pptn. of the excess phase. A. H. Krappe

ASH-SLA METALLURGICAL LITERATURE CLASSIFICATION

VOLUME SYMBOL

CLASSIFICATION

EIGHT-CHARACTER

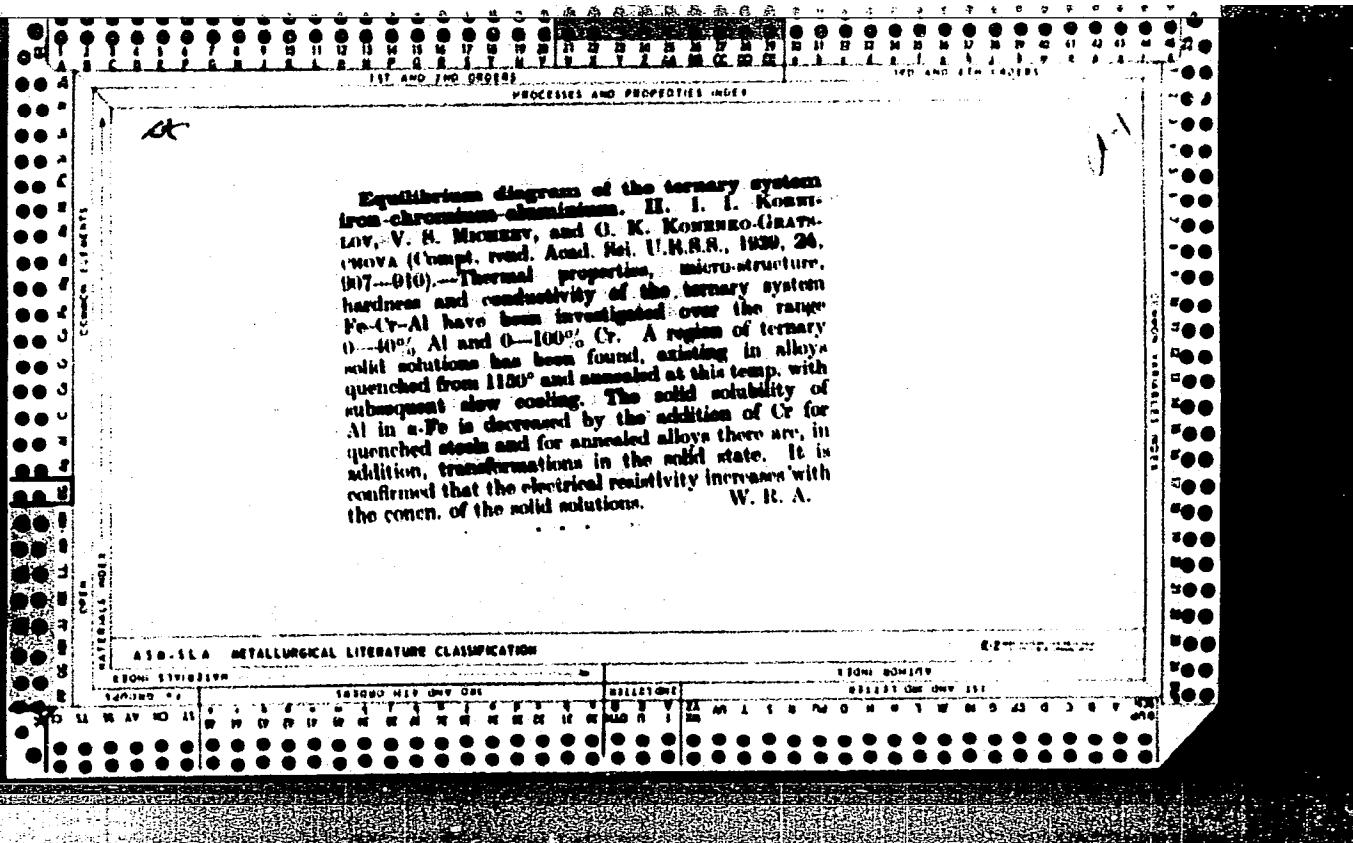
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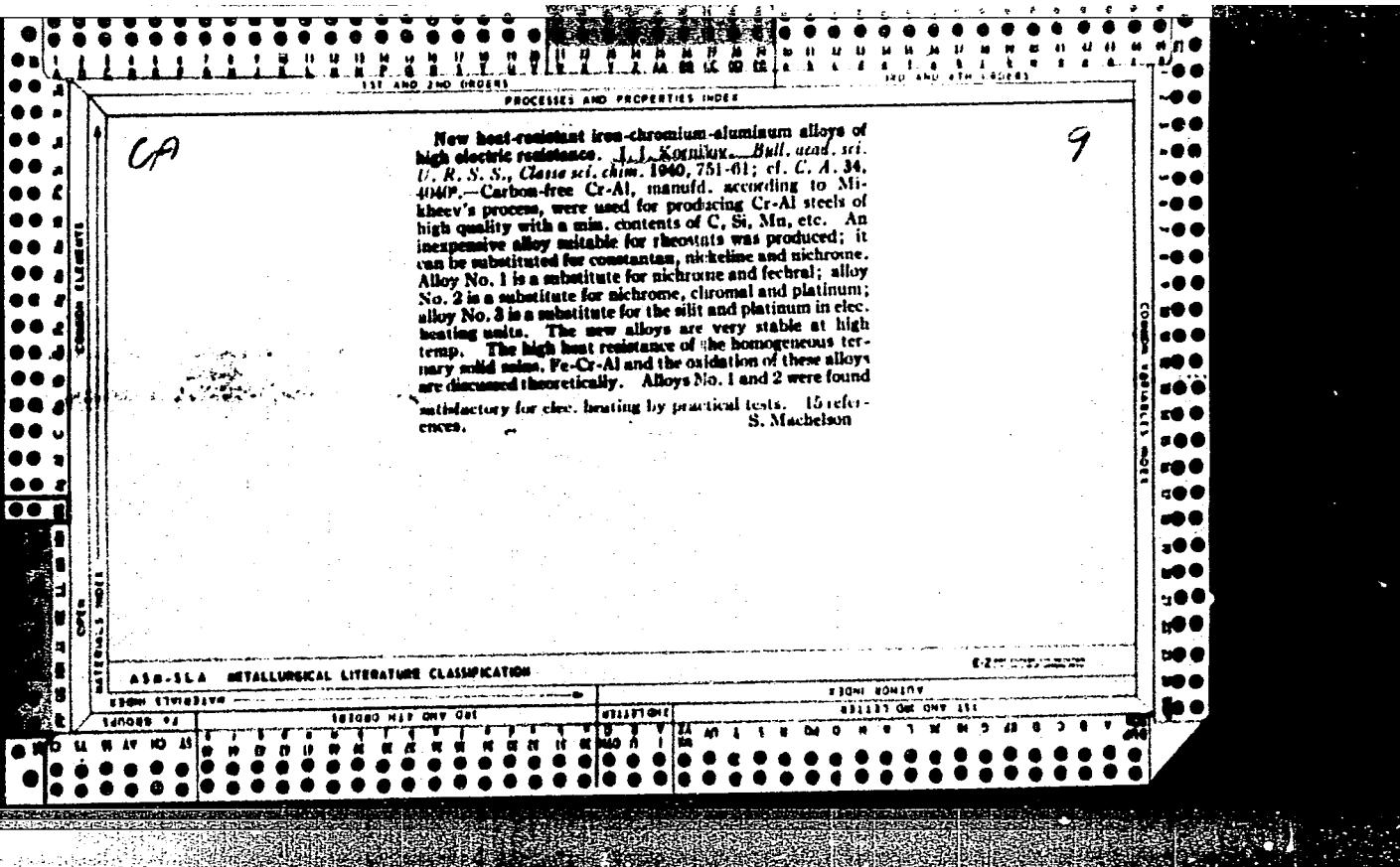
Technology of new heat-resisting elements—chromium steels of high electrical resistivity. I. L. I. Kozairov, III. I. I. Kuznetsov and U. N. Mischenko (Gauge, rend. Akad. Nauk. U.R.S.S., 1959, 54, 914-920, 911-914; v. It., 1960, 1049; A., 1960, 1, 156).—I. Four groups of Cr-Al-V alloys of high sp. electrical resistance, low temp. coeff. of resistance, and high heat-resistance are described. They are case, homogeneous solid solutions of Cr and Al in ϵ -Fe and their high heat-resistance is attributed to the formation of a homogeneous surface film of Al_2O_3 , Fe_3O_4 , and Cr_2O_3 in solid solution. Possible uses of these alloys are listed.

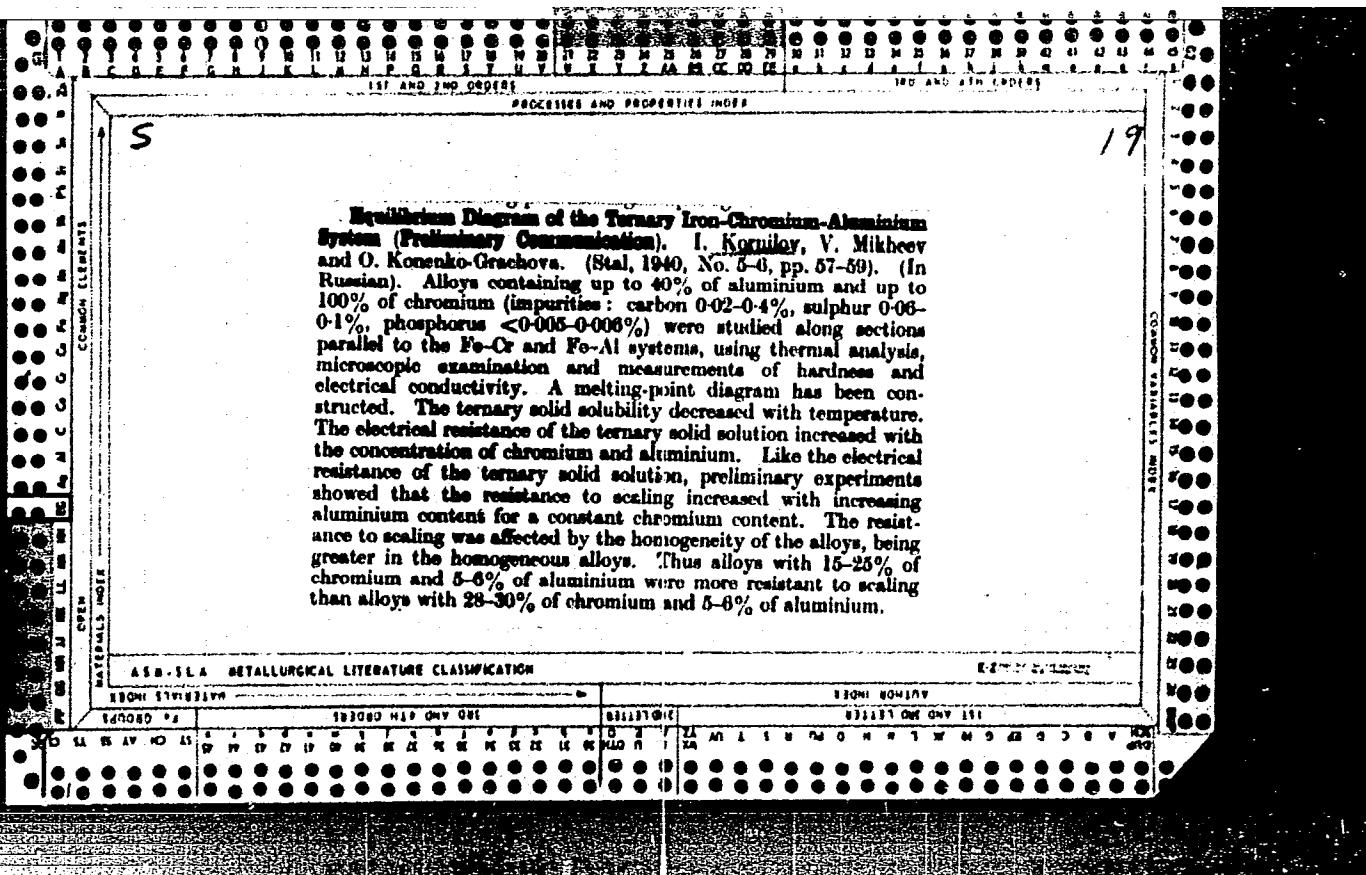
III. An aluminothermic method has been developed by which Al-Cr and Fe-Cr-Al alloys are prepared by combining the process of melting the Fe in oxygen with reduction of Cr oxide and Cr ore consumption by excess of Al. By this method Al-Cr steels of any desired composition (Al > 30%) have been prepared. These steels contain very much less C, Si, Mn than those prepared by adding Al at the end of the steel-smelting process, and, in addition, less oxidation of the Al occurs and more homogeneous distribution of the Al results. Slags of CaO , MgO , and Al_2O_3 were used in smelting the new Cr-Al steels. The thermal and electrical resistance of these new steels is high. Typical specimens, e.g., Cr 10-50, Al 0-20, Fe 60-68 and 60-68%, are discussed; these contain ~8-10 times less C and 3-4 times less Si than do chromial or ferrite steels containing Cr 10-50 and Al 0-10%. They can be forged, but alloys with 20% Al cannot be forged, although they give uniform solid solutions.

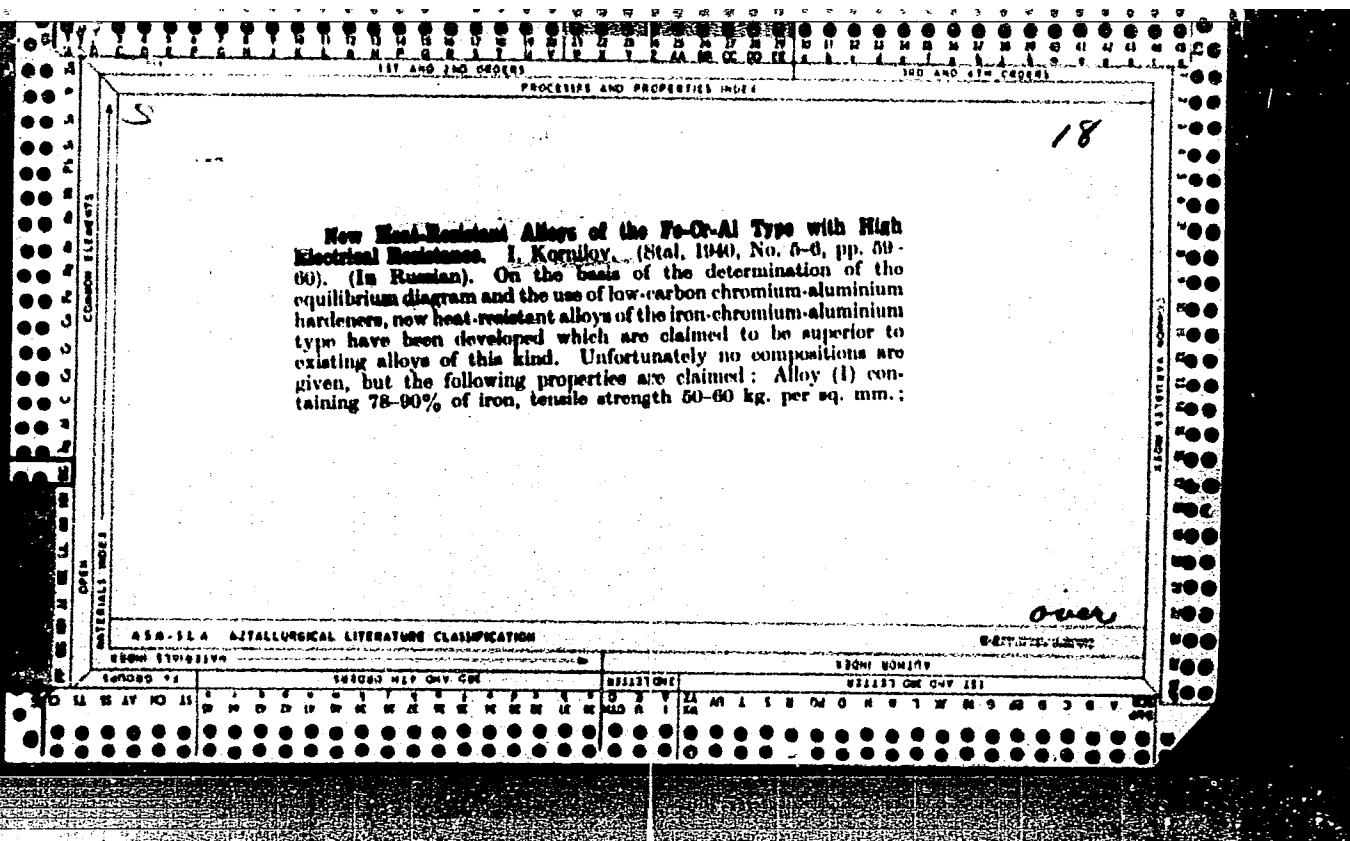
Steels with Cr > 45 and Al > 10% can be hot-rolled to 5-mm. wire, ribbon, etc. Steels with an Al content > that of chromal can also be cold-rolled. Although rather brittle at room temp., the steels become plastic at 200-400°. The use of these steels as substitutes for nichrome and Pt as electric heating elements and as substitutes for high-resistivity steels is indicated.

W. R. A.









elongation 18-25% ; working temperature 1000-1100° C. ; specific electrical resistance 1.40-1.60 ohms per sq. mm. section per m. length; temperature coefficient of resistance 0.00006. Alloy (2) containing 68-69% of iron, tensile strength 60-65 kg. per sq. mm.; elongation 18-20% ; working temperature 1200-1250° C. ; specific electrical resistance 1.45-1.70 ohms per sq. mm. per m. ; temperature coefficient 0.00004. Alloy (3), containing 60-65% of iron, working temperature 1350-1400° C. ; specific electrical resistance 1.70-1.90 ohms per sq. mm. per m. ; temperature coefficient 0.00003. A rheostat alloy was also developed; this contains 85-90% of iron, has a working temperature of 600-800° C. and a specific electrical resistance of 1.20-1.40 ohms per sq. mm. per m. Alloys (1) and (2) and the rheostat alloy can be cold- and hot-worked. Alloy (3) can only be hot-worked. The hot-drawing of alloy (3) into wire is now being developed. All these alloys can be gas and are welded. A 1/1 mixture by weight of CaF₂ and KCl is recommended as a flux for welding.

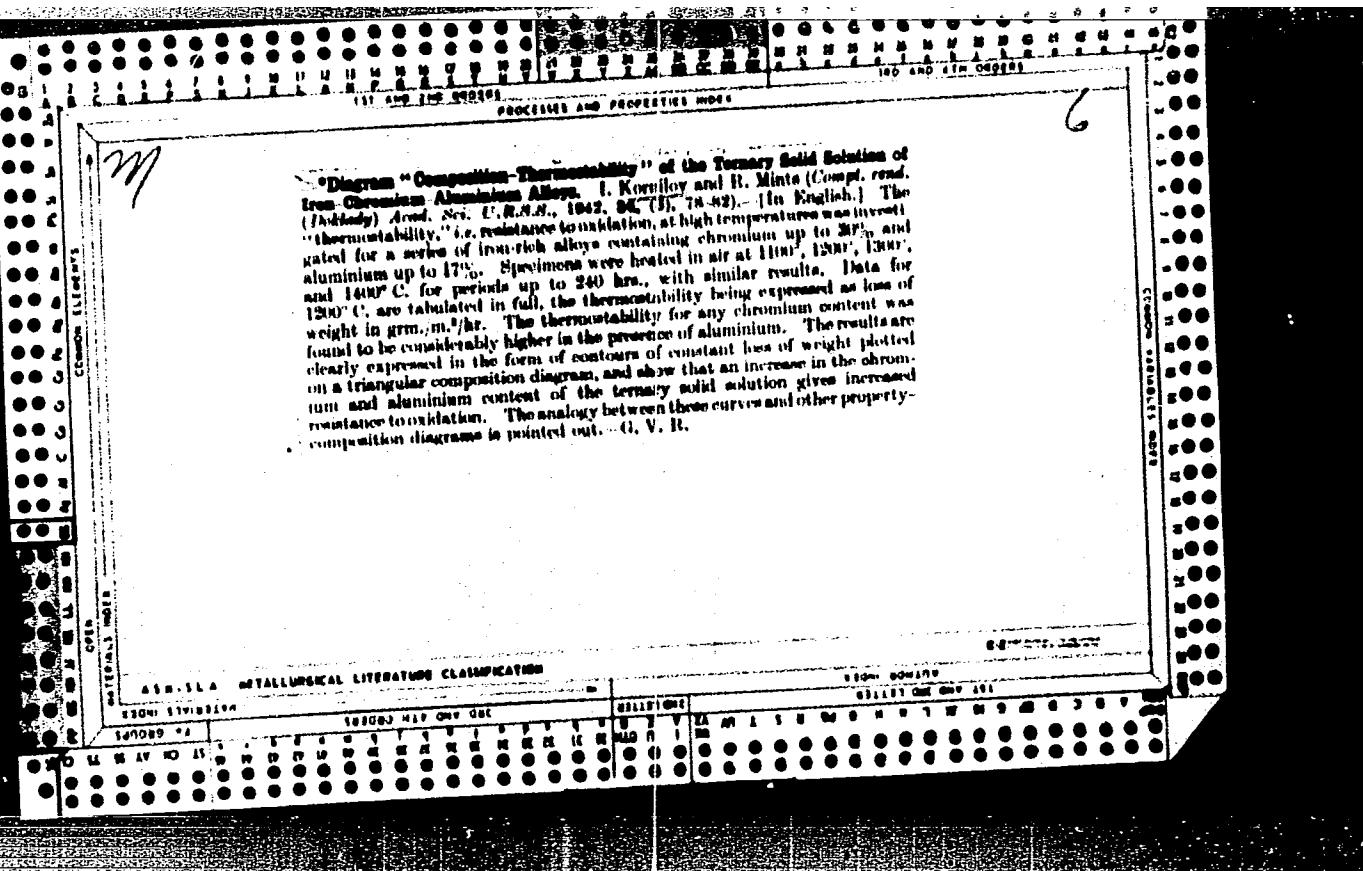
KORNILOV, I. I.

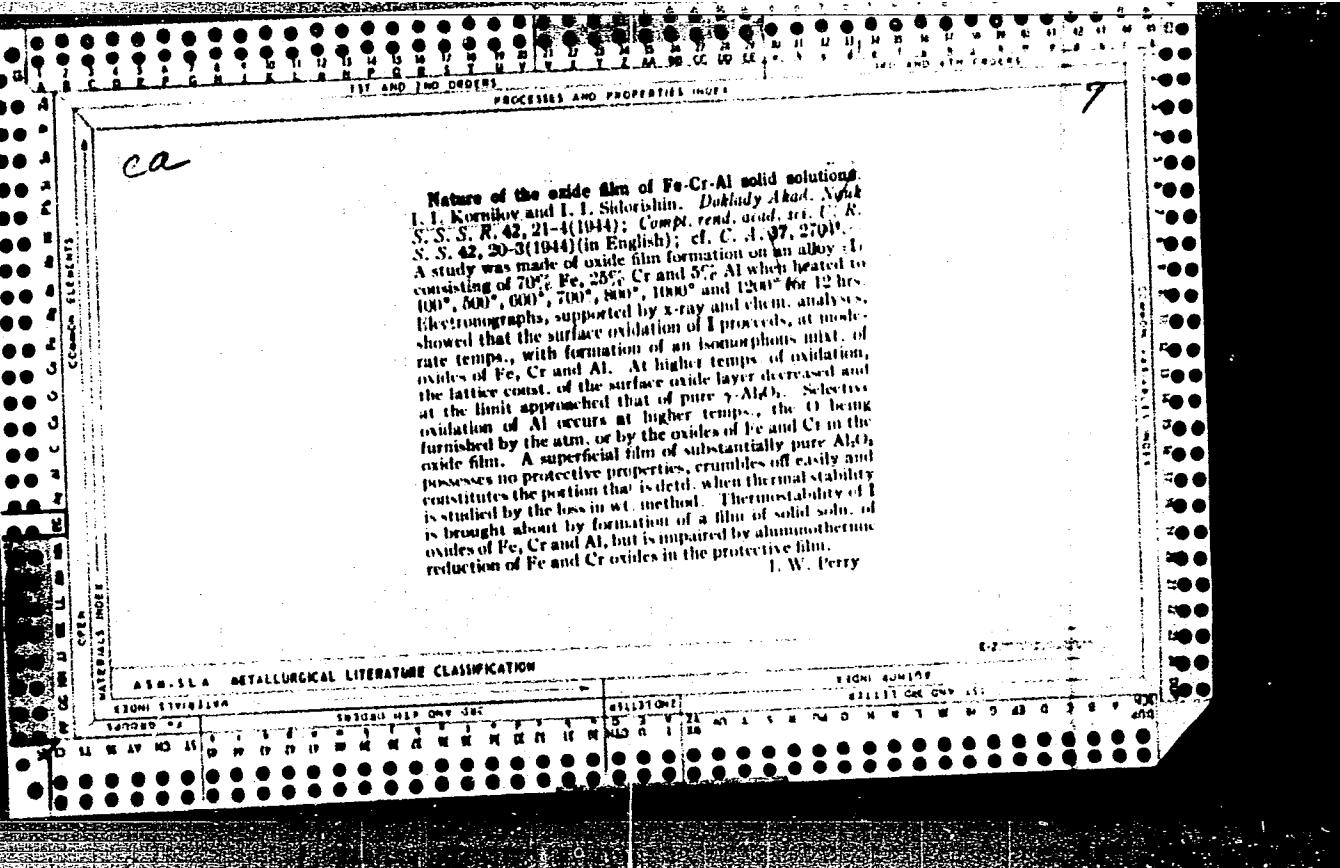
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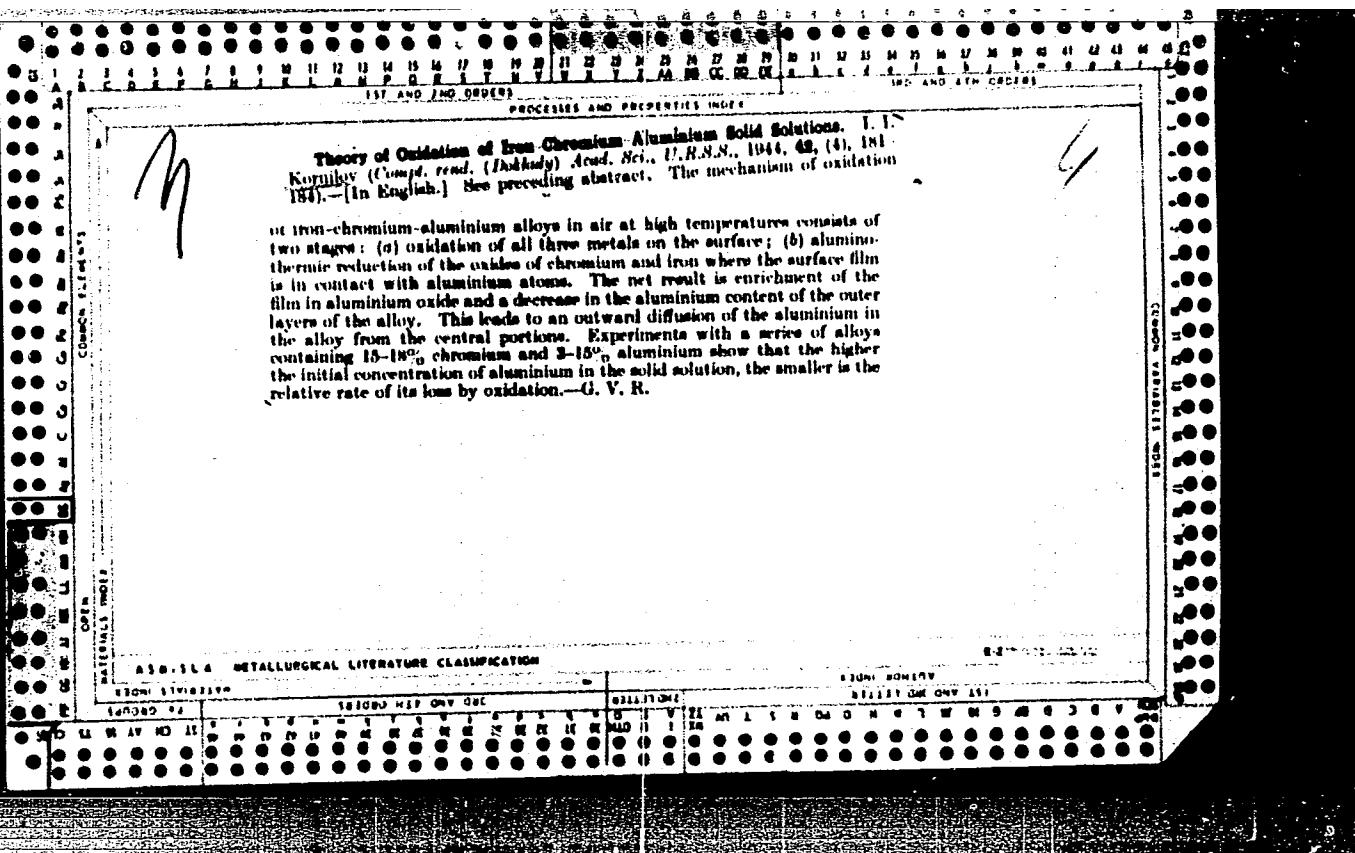
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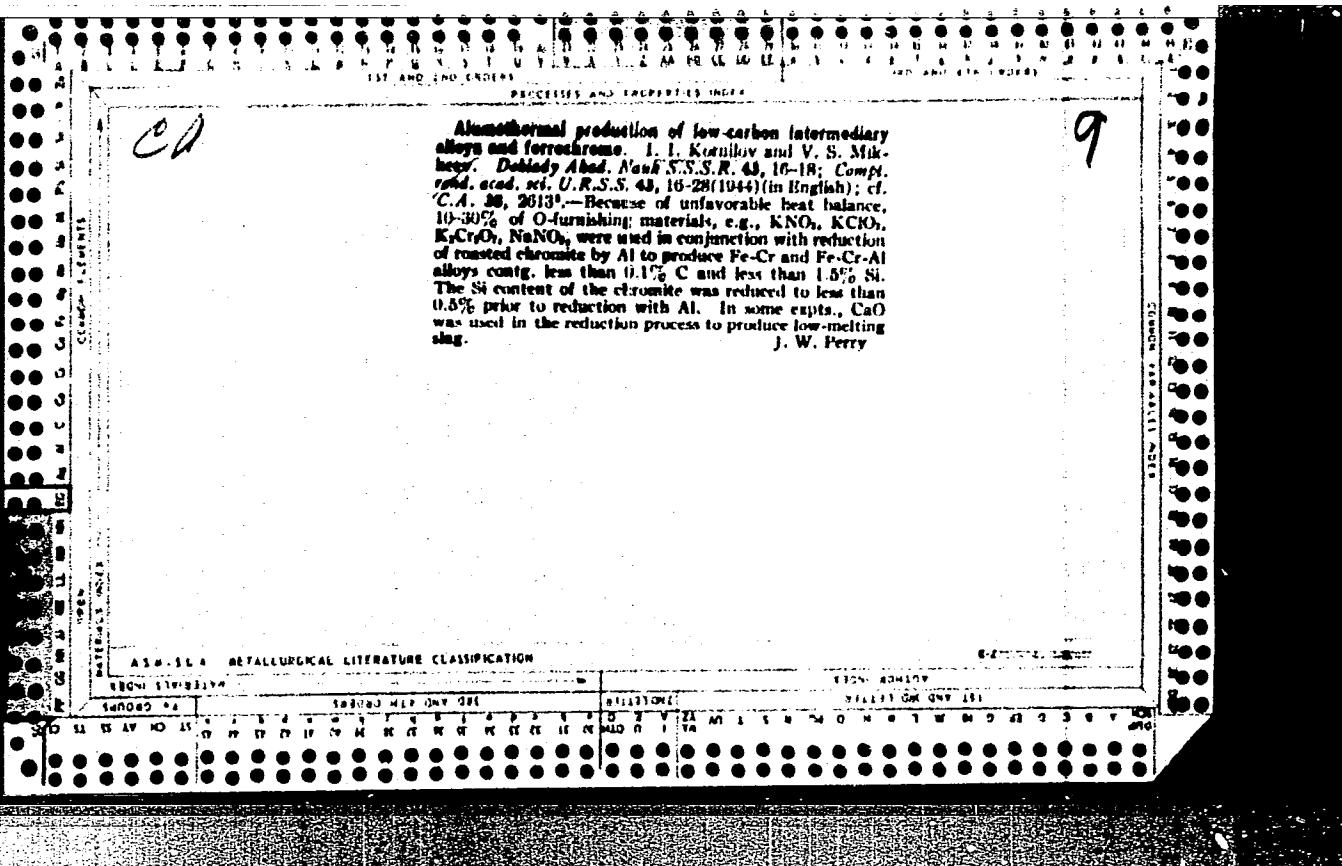
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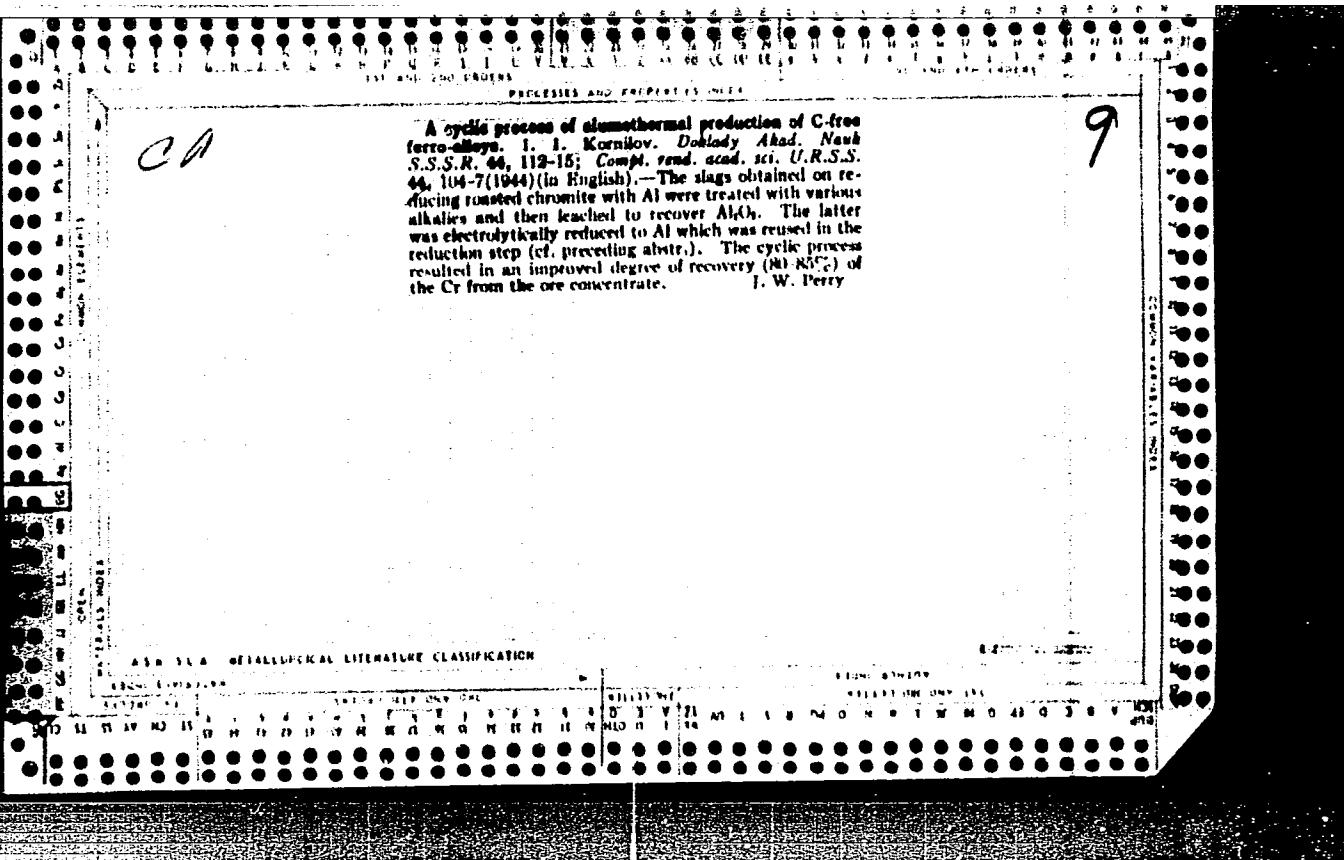
I. I. Kornilov and V. Mikhayev, Commercial Production of New Chrome-Aluminum Steels with the Use of Key Alloys. STAL, vol. 10, 1940, pp. 14-18; 4900 words.









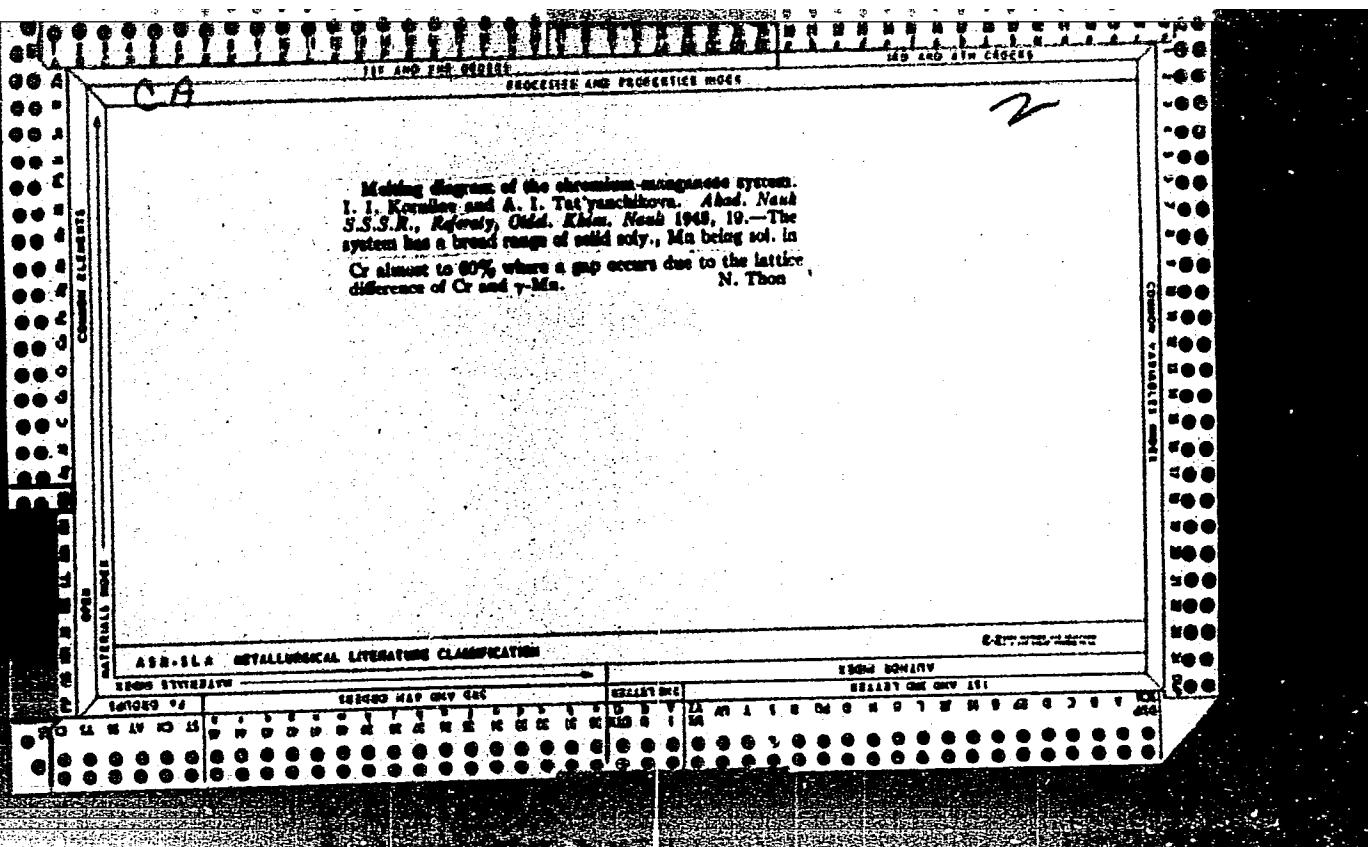


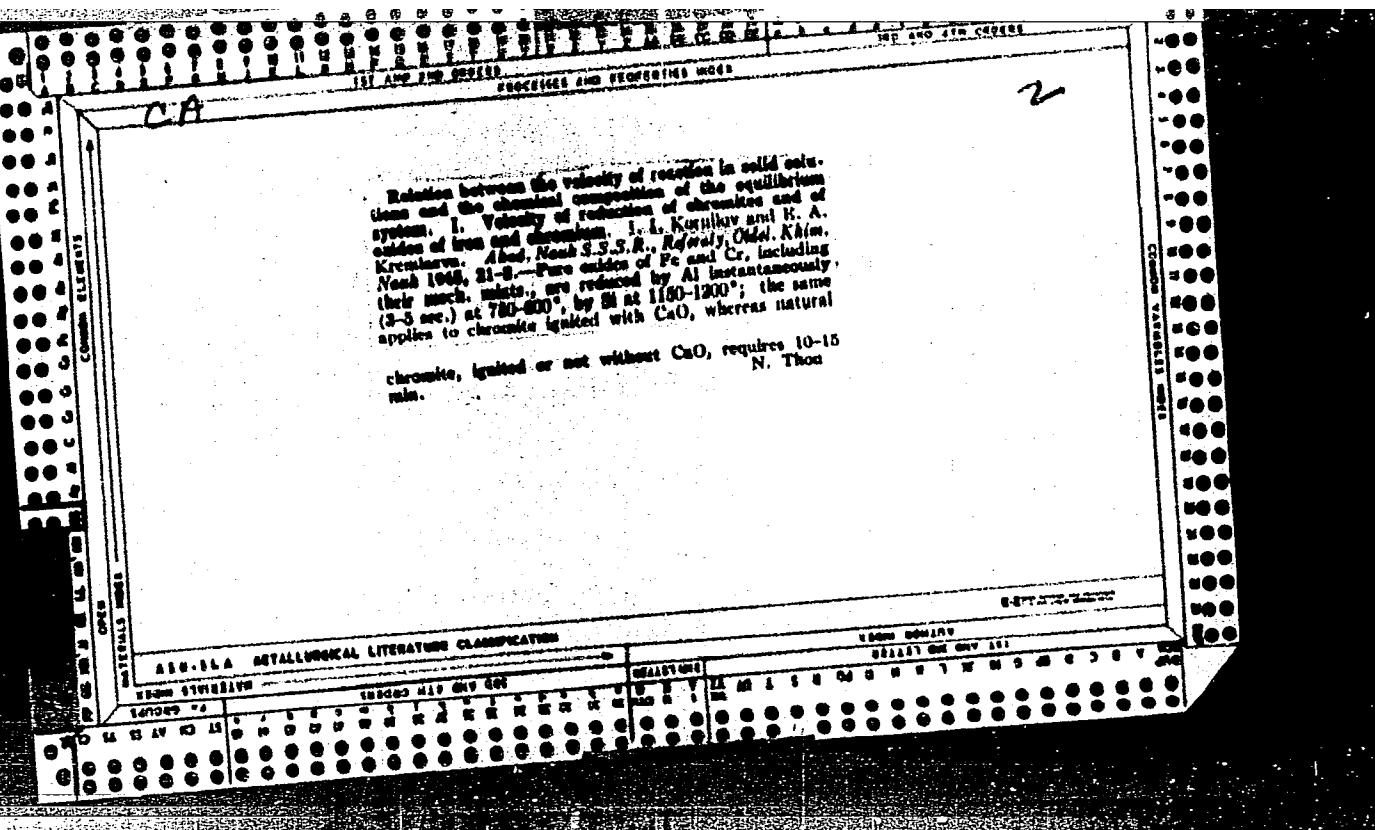
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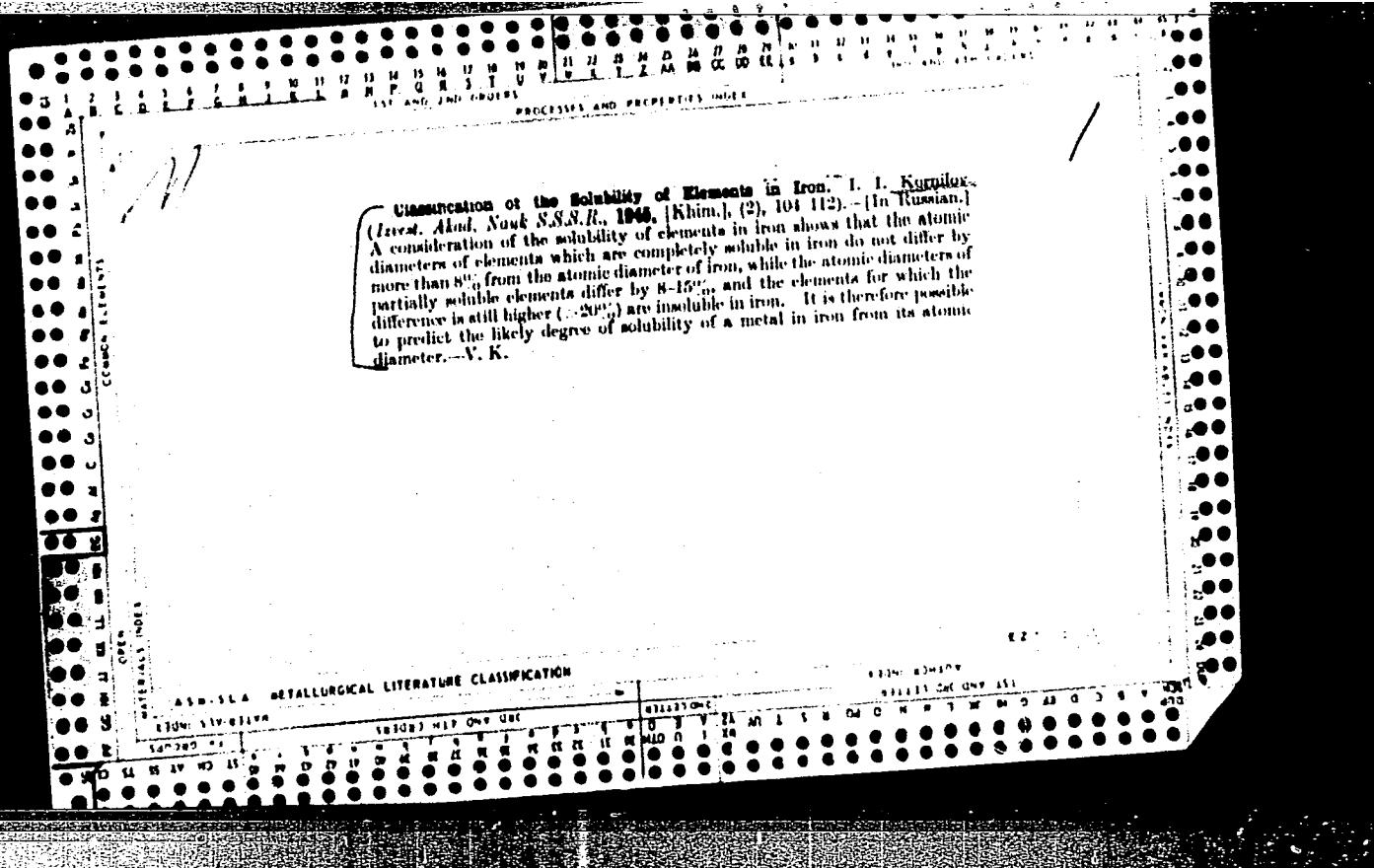
Iron-Chromium-Aluminum Alloys, Published by Academy of Science, Moscow 1945.

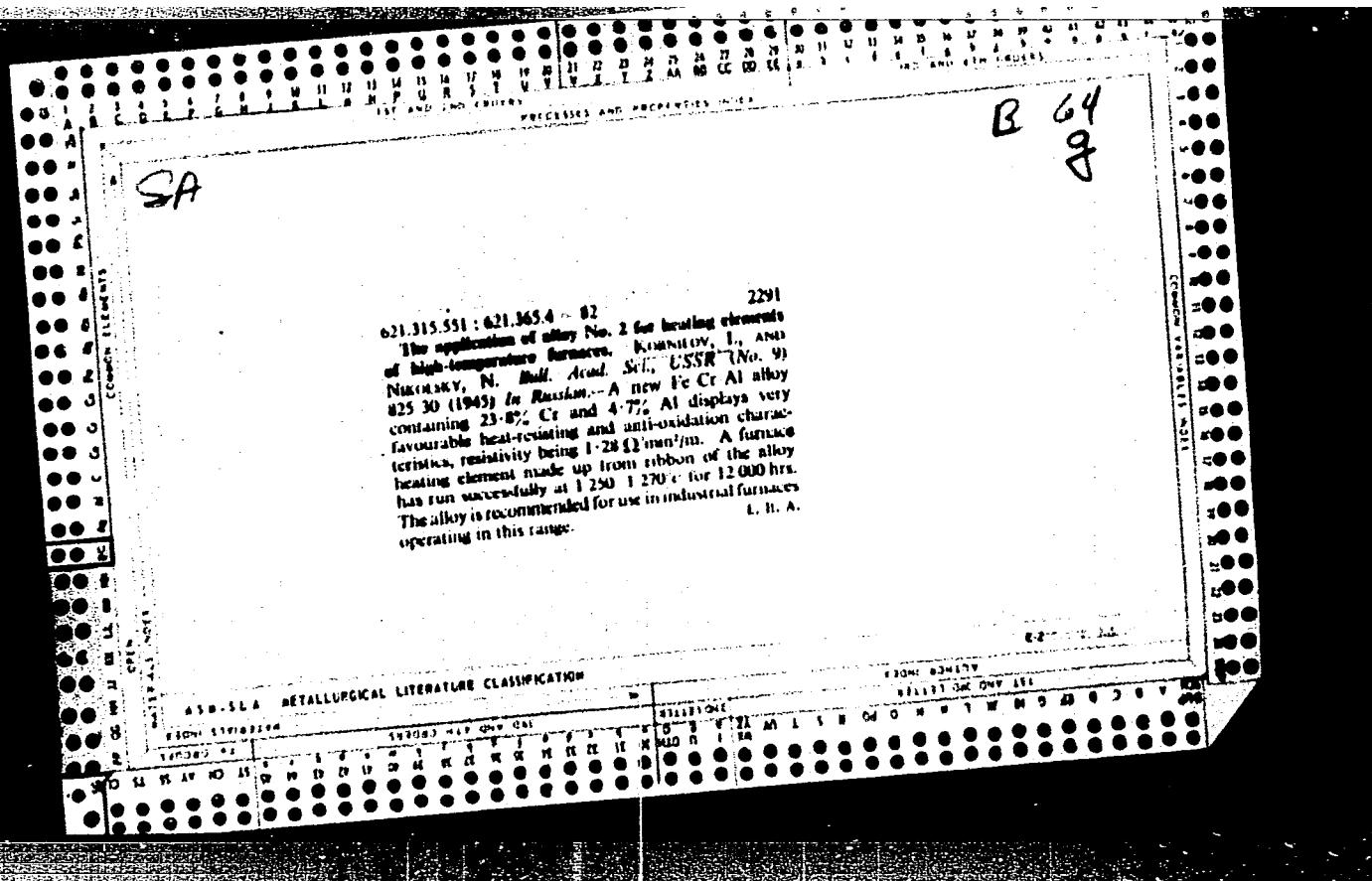
Institute of General and Inorganic Chemistry, Laboratory of the Iron Alloys.

B-68125, 1 Sep 53









CH

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Melting diagram of the chromium-manganese system.
I. I. Kornilov and A. I. Tat'yanchikova. *Doklady Akad.*
Nauk S.S.R. 30, 223-5(1945); cf. *C.A.* 42, 62191.—
In a study of the melting region of the Cr-Mn system use
was made of electrolytic Cr with 0.01 C, 0.02 Fe, and
0.02% Si, and electrolytic Mn with 0.01 C, 0.002 Fe,
0.04% Si, and no Si. The alloys were melted in fused
Al₂O₃ crucibles in an induction furnace. Cooling curves
were obtained for 14 compas. from 30.9 to 100% Mn, and
the thermal arrests and microscopic appearances are tabu-
lated. Only microscopic studies were made of three
higher-melting compas., 27.2, 14.4, and 8.7% Mn.
Addnl. data were obtained by heating alloys to 1100° in
vacuum for 24 hrs. and then quenching in H₂O or furnace
cooling in vacuum during the course of 48 hrs. The
liquid-solid reaction consists of a peritectic horizontal at
1360° extending from about 70 to 80% Mn, and joined by
solid soln. reactions to the m.p. of Cr and of Mn. The
Cr solid soln. is interrupted by transformation into the
CrMn intermetallic compd. at about 50% Mn. Two
solid reactions are shown, a peritectoid horizontal at about
1000° extending from about 85 to 93% Mn, and a eutec-
toid horizontal at about 650° extending from about 70
to 85% Mn. The limit of solv. of Cr in Mn after anneal-
ing is 5%. The eutectoid structure is like that of pearlite.
A. G. Gay

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✓ Mechanical Properties of Kevlar® Aramid Fibre
Binary Alloys

0.5% elongation at break up to 10% strain rate

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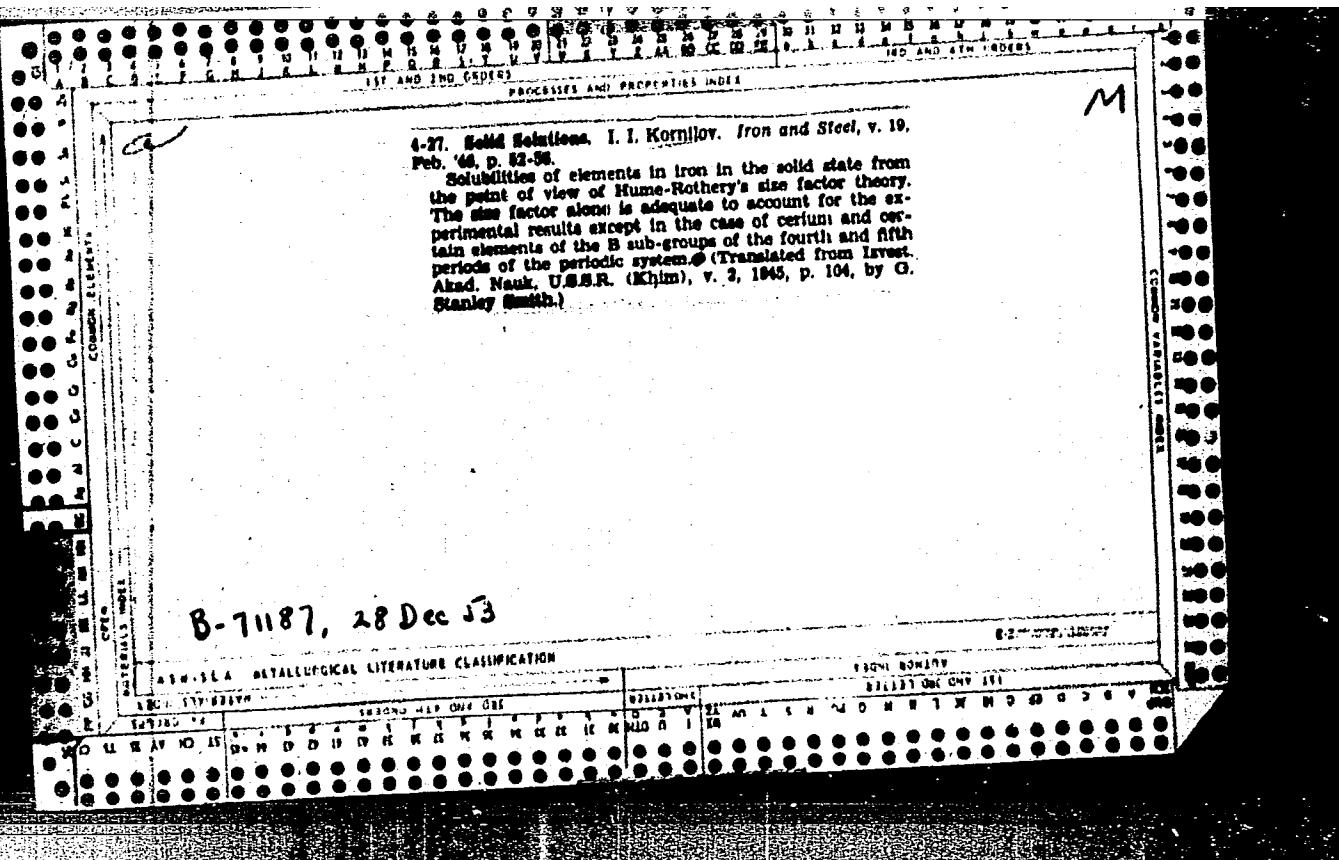
Laboratory resistor furnaces with resistors of "alloy No. 3." I. I. Kornilov and A. V. Kuz'min. *Zagotokay Lab.* 12, 87-138(1940); cf. C.I.I. 41, 26464. The alloy is used as substitute for nichrome in resistor furnaces. At 1000°, coils made of alloy No. 2 last as long as, and in some cases longer than, nichrome coils. The max. temp. tolerated is 1250°. The No. 2 alloy coil contains Al more than 4.5%, & less than 10.8%. Resistivity of the wire is 1.3-1.4 ohms/sq. mm./cm. At 1000° the alloy reacts noticeably with Si and Fe. The coating on the coil should contain not over 10% Si and not over 3% of Fe_3O_4 . The coating consists of Al_2O_3 50, grog (ground to 3 mm.) 30, and grog clay 20%. The mass is dried before use at 180-200° until hardened. W. R. Henn

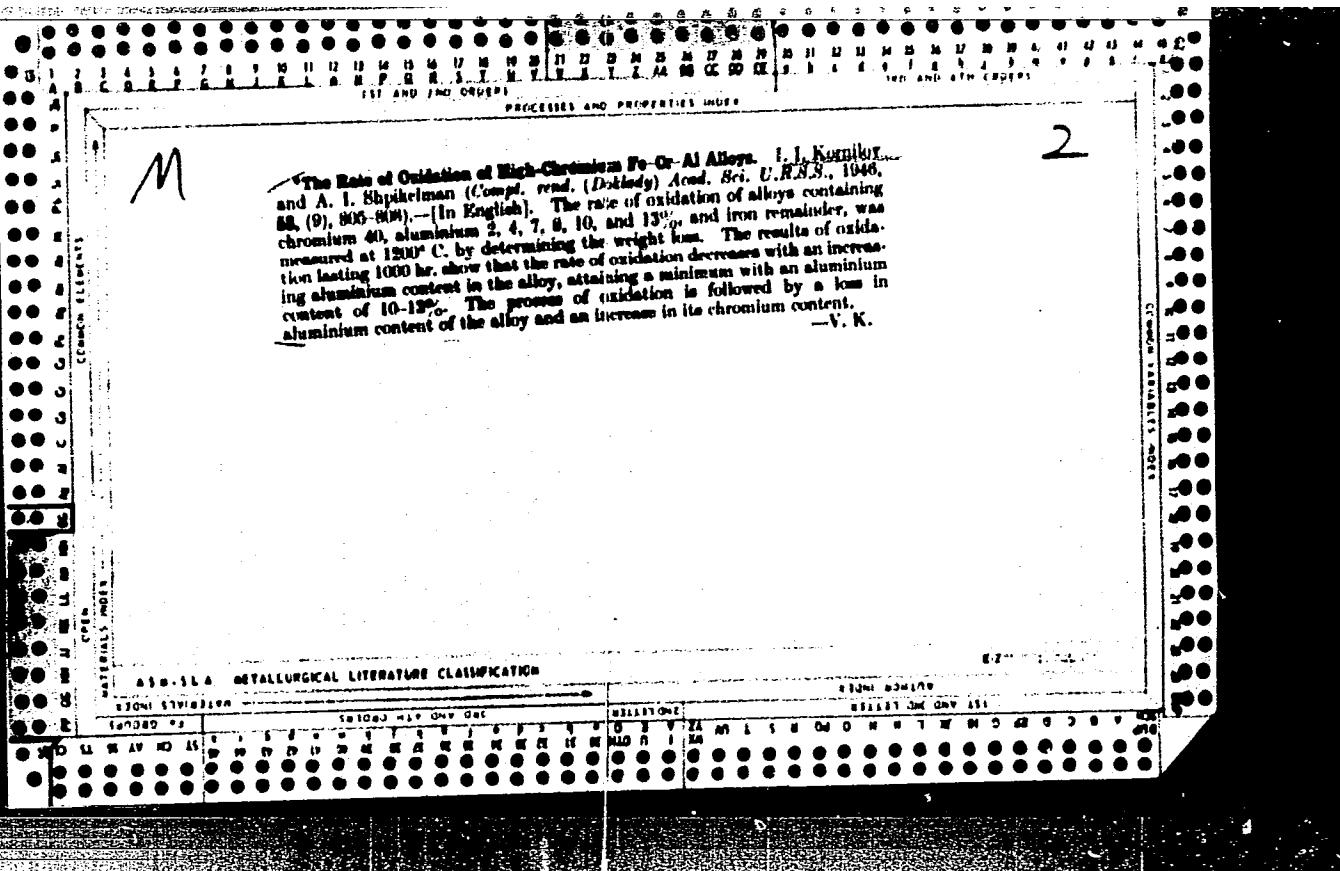
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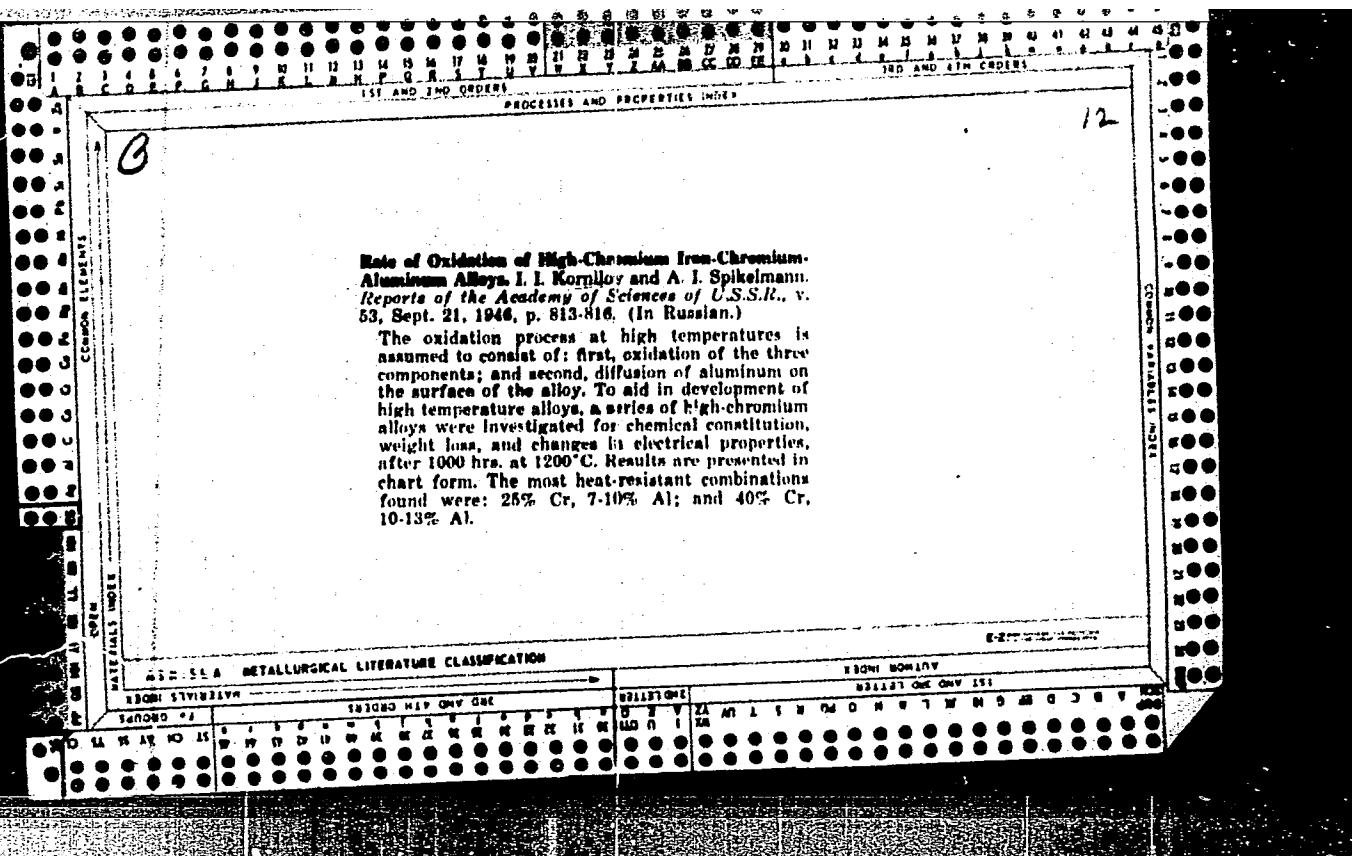
AIA 51-4 METALLURICAL LITERATURE CLASSIFICATION

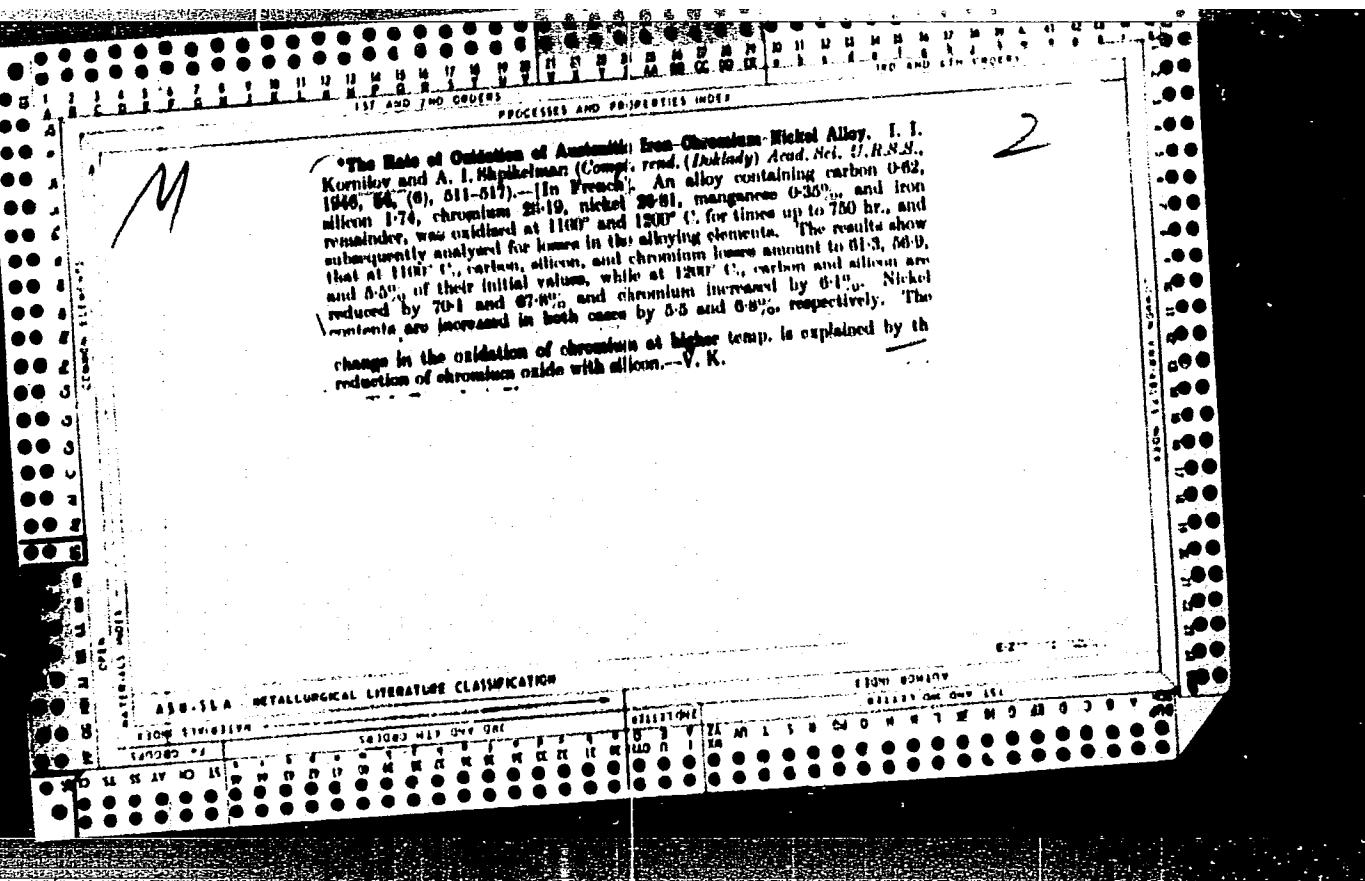
CH

Equilibrium diagram of the ternary system iron-chromium-aluminum. A. I. Kozachenko, V. S. Mikheev, O. K. Koneenko-Gracheva, and R. S. Mintus. *Izvest. Akad. Nauk S.S.R. Fiz.-Khim. Anal., Inst. Obshchel i Neorg. Khim.*, No. 2, 100-15 (1940); cf. *C.A.* 34, 4041; 42, 5396. — The object of this study were alloys with up to 100% Cr and up to 60% Al. The most significant of these were ternary alloys forming a solid soln. of the 3 components and designated as α_1 . The boundary of α_1 was traced on a phase diagram. The electroresistance of α_1 increased more with an increased Al content than with a rise in the Cr content. As the Al and Cr increased, the temp. coeff. of the electroresistance decreased. At a const. Cr content, Al increased the dilation of the alloys, whereas Cr decreased thermal dilation. M. Ilseh









KORNILOV, I. I.

1ST AND 2ND ORDERS

3RD AND 4TH ORDERS

PROCESSES AND PROPERTIES INDEX

Speed of oxidation of the austenite-type iron-chromium-nickel alloy. I. I. Kornilov and A. I. Sosulin [mag.]

Compt. rend. acad. sci. U.R.S.S. 84, 611-14 (1950) (in French); cf. *C.A.* 41, 37304.—The preferential speeds of the various elements in an alloy of the B X H type contg. C 0.02, Si 1.74, Cr 28.19, Ni 26.81, Mn 0.35, Fe 42.29%, which possesses a high thermal stability, were investigated at temps. of 1100° and 1200° over a period of 750 hrs. with round bars 60 mm. long and 8 mm. in diam. The loss of wt. and variations in the percentage compn. were detd. for each temp. after 120, 240, 500, and 750 hrs., to investigate the role of each element in the oxidation. A table gives the speed of oxidation, expressed as percentages of the original content of the alloy. As was

the case with the ferrites previously reported, the austenite-type thermostable iron alloys are oxidized at high temps. principally at the expense of the elements easily oxidized. In the former alloys, it is at the expense of the Al, while in the austenite type, the C, Si, and Cr play the important role up to temps. of 1100° to 1150°. If the temp. is increased above 1200°, the C and Si alone undergo oxidation.

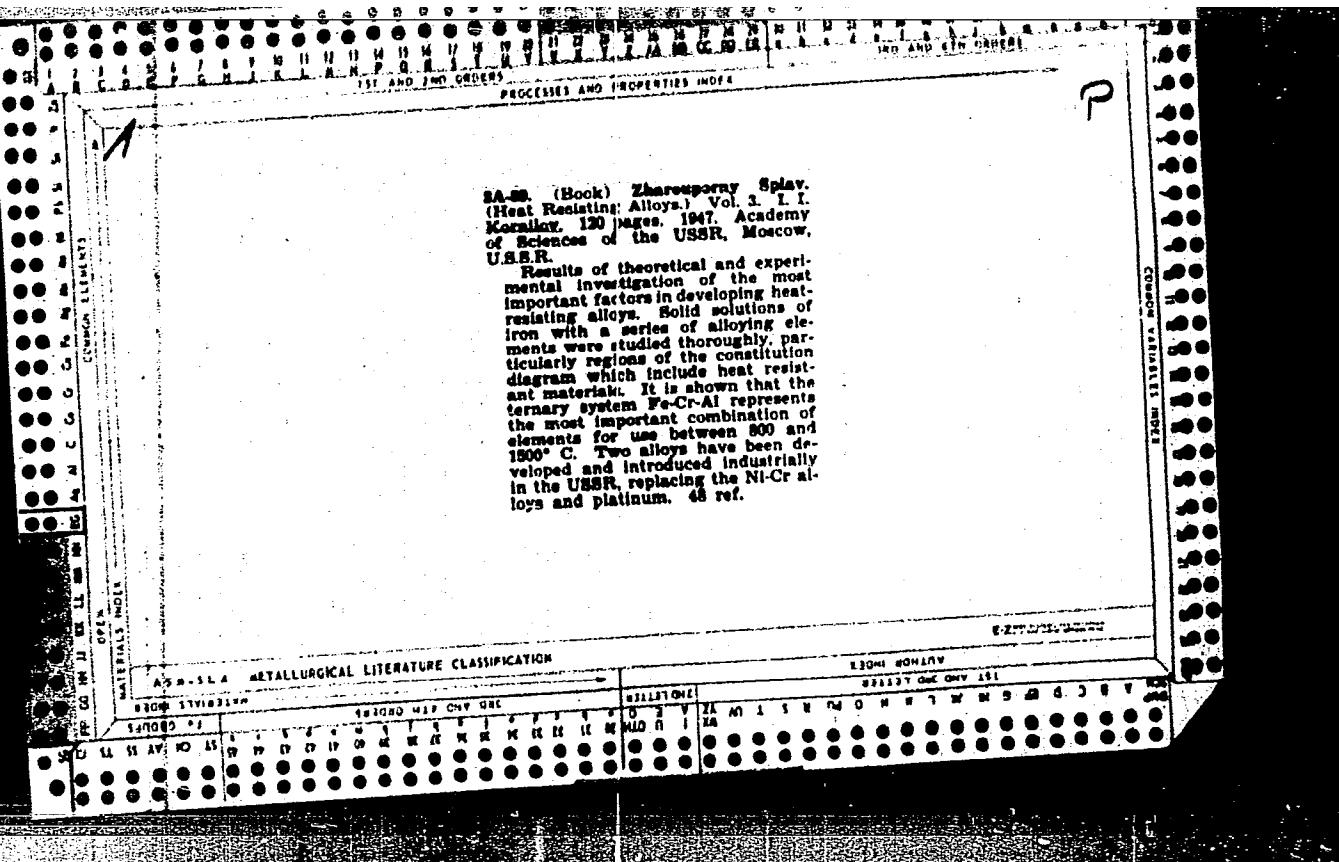
Helen F. Pool

KORNILOV

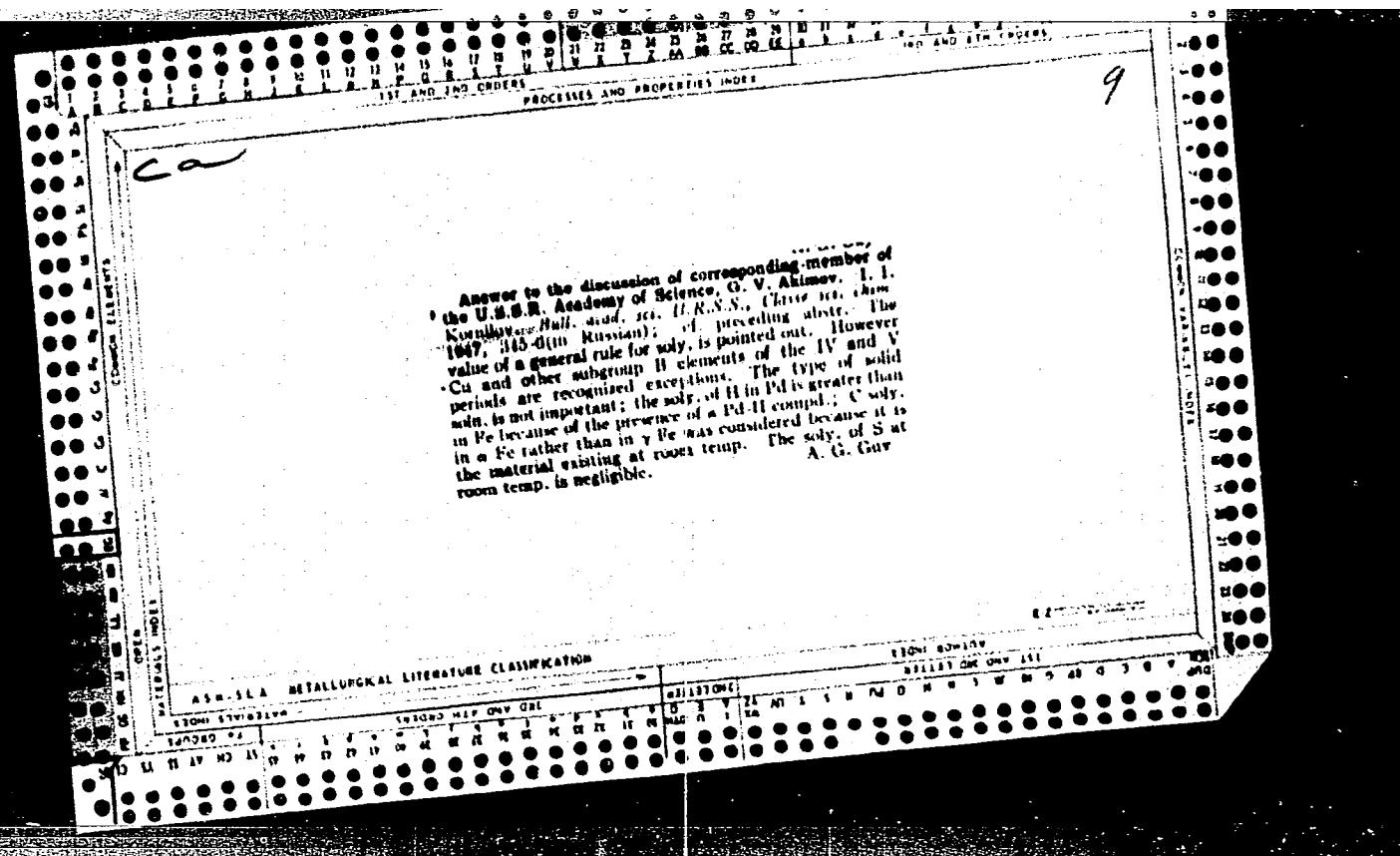
1ST AND 2ND GROUPS
PROCESSSES AND EQUIPMENT INDEX
"The Rate of Oxidation of High-Chromium Yu Al Alloys" I. I. Kostylev
and A. I. Shpilevman (Uspol. zvezd. (Moskva) Acad. Nauk P.R.S.S. 1940,
No. 19), with sum. (In English). The rate of oxidation of alloys containing
chromium 40, aluminum 2, 4, 7, 9, 10, and 12% and iron remainder, was
measured at 1300° C. by determining the weight loss. The results of tests
lasting 1000 hr. show that the rate of oxidation decreases with an increasing
aluminum content in the alloy, attaining a minimum with an aluminum
content of 10-12%. The process of oxidation is followed by a loss in
aluminum content of the alloy and an increase in its chromium content.

KORNILOV

ALUMINA METALLURGICAL LITERATURE CLASSIFICATION



PROCESSES AND PROPERTIES INDEX		
<p>KORNILOV</p> <p>CONTINUOUS SOLID SOLUTIONS OF ELEMENTS IN IRON</p> <p>The classification of the solubilities of elements in iron. I. I. Kornilov. Bull. acad. sci. U.R.S.S., Classe sci. chim. 1947, 337-343 (in Russian); cf. C.A. 39:5144. —Chem. elements having the same cryst. lattice as Fe and differing in at. diam. by not more than 8% can form a continuous series of binary solid solns. with Fe. Since Fe can form solid solns. based on the α-Fe lattice (ferrite) or on the γ-Fe lattice (austenite), the 8 elements that can form continuous binary solid solns. with Fe are divided in this manner. Cr and V are the only elements that form continuous binary solid solns. of the ferrite type. Since it has been reported that there is complete solid solv. in the Cr-V system, it is supposed that the ternary system Fe-Cr-V shows continuous solid solv. A hypothetical diagram is shown with the solid-solu. region broken by the γ loop and by the compds. FeV and FeCr. The elements Co, Ni, Rh, Pd, Ir, and Pt form continuous binary solid solns. of the austenitic type. A total of 15 ternary continuous solid-solu. systems of this type are possible. The solid-solu. region in each of these ternaries is interrupted by the $\alpha \rightleftharpoons \gamma$ transformation, and in all except possibly the Fe-Ni-Co system chem. compds. form in the solid state. The mode of occurrence of both of these discontinuities in the solid solv. is shown schematically for the Fe-Ni-Pt system. A total of 20 quaternary austenitic continuous solid-solu. systems involving Fe is</p> <p style="text-align: right;">9</p>	<p>possible, and a tetrahedral representation of the $\alpha \rightleftharpoons \gamma$ transformation in a typical system is given. Eleven quaternary systems are possible. 20 references. Discussion. G. V. Akimov. Ibid. 34:4-5 (in Russian). —The conclusions stated by K. are criticized. It is pointed out that differences in at. diam. are not always sufficient to det. solid solv., as in the case of Fe-Cu, where the diams. are almost identical but the solid solv. is slight. Although these geometrical factors are significant in substitutional solid-solu. formation, they cannot be applied to interstitial solid solns. It is suggested that there is some solid solv. of Fe for S.</p> <p style="text-align: right;">A. G. Gav</p>	
ASH-SLA METALLURGICAL LITERATURE CLASSIFICATION		
X104.51918315.0		E-2171772-A0000
SOLID STATE PHYSICS		ADDITION INDEX
SUBSTITUTIONAL SOLIDS		1974 AND 1975 LETTERS
INTERSTITIAL SOLIDS		X11133 Q171



CA

Composition and properties of refractory alloy No. 3
high electric resistance. I. I. Kornilov and A. A. Azovskaya. Vestn. Mashinostroyeniya 27, No. 5, 71-2 (1947);
Chern. Zvezd. 1948, II, 912-13.—The ternary alloys No. 1 and 2 (Fe-Cr-Al) were tested as materials for resistances of elec. furnaces. These are unsatisfactory up to 1200°. The refractory alloy No. 3 (Fe-Cr-Al) has been developed which withstands temp. of 1300-50° without essential oxidation or other damage. Sp. resistance, tensile strength, and elongation were measured on alloys contg. 40% Cr and 0-12% Al (series I) and those contg. 25% Cr and 0-12% Al (series II) to det. the effect of the Al content on these properties. The tensile strength of all alloys of series I was considerably higher than that of those of series II. It increased progressively with the Al content. In tensile tests on series I the elongation was 10% at 0% Al content; II the elongation was 20-25% at 5.5-6% Al. Above 6% Al the elongation dropped sharply and the alloys became brittle at room temp. Impact tests showed those heat-resistant alloys having a high sp. elec. resistance to be brittle at room temp. Alloys contg. 40.8% Cu and 7.3% Al remained brittle even when heated to 900-1000°. The impact resistance of the alloy contg. Cr 27.2 and Al 7.0% increased considerably between 300 and 400°. Alloy No. 3 recommended could be worked at 300-400°. Alloy No. 3 is recommended as a resistance material for temps. of 1300-1350°. It contains C 5.00, Cr 23-7, Al 4-8, Si 1, Ti 0.2-0.4, S 0.02, and P 0.03%. Its elec. resistance is 1.45-1.60 ohm-sq. mm. per m. Heating this alloy to 750° for 30-40 min., and quenching in water reduced the tensile strength from 40-100 to 75-85 kg./sq. mm. and at the same time increased the elongation from 3-8 to 10-15%. Hot-rolled ribbons 2 X 20 mm. and wires 6 mm. in diam. could be produced from alloy No. 3. These products could be used for the resistances of elec. furnaces without the need of a transformer.
M. G. Mowre

KORNILOV, I. I.

Rate of oxidation of quaternary alloys of iron-chromium-nickel and manganese. I. I. Kornilov, A. T. Durnov, and
I. I. Pavlovina. Doklady Akademii Nauk S.S.R. 58,
1000-8 (1947).—Oxidation rates of alloys contg. 17.3-20.5%
Cr, 7.8-9.2% Ni, 10.7-2.85% Mn, and 68.2-68.5% Fe
were detd. The results, given graphically, indicate that
at 1000° alloys contg. Mn and Fe oxidize more rapidly
than those contg. Cr or Ni. In order of rate of oxidation
the series is Mn, Fe, Cr, and Ni. Most of the oxidation
falls to Mn and it detns. the general rate of reaction. Ap-
parently Mn_2O_3 , Fe_2O_3 , Cr_2O_3 , and NiO are the products.
 MnO and Fe_3O_4 are unstable oxides under conditions of
alternate heating and cooling and they do not form a pro-
tective film.

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③

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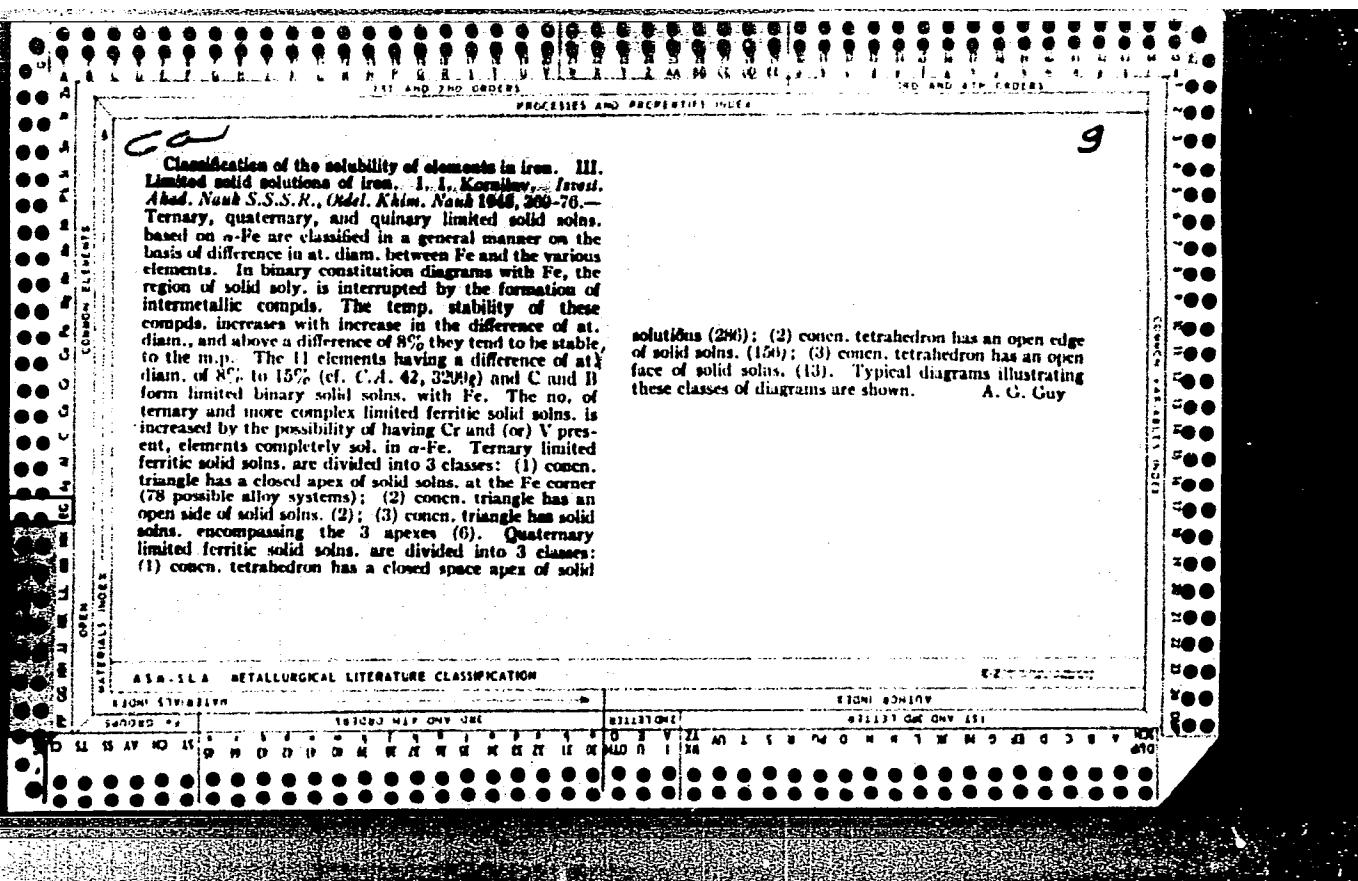
KORNILOV, I. I.

"Experiments in the Application of the New Iron-Chrome-Aluminum Alloys for Heating Elements," Elektrichestvo 67, No 2, 1947

Prof., Inst. Gen. and Inorganic Chemistry, AS USSR

APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R000824720006-2"



KORNIL'OV, I. I.

IA 6/49T10

USSR/Chemistry - Iron, Solid Solution
Chemistry - Solubility

Jul/Aug 48

"Classification of the Solubility of Elements in
Iron," I. I. Kornilov, Inst Gen and Inorg Chem
imeni N. S. Kurnakov, Acad Sci USSR, 6 3/4 pp

"Iz Ak Nauk SSSR, Otdel Khim Nauk" No 4

Defines group of elements with a difference of
8 - 15% in atomic diameters, forming double
limited solid solutions with iron beginning
with ratio of atomic diameters to iron. Gives
systematism of triple, quaternary and more complex
limited solid solutions of ferrite on basis of these
elements. Calculates the number of possible systems.

8/49T10

USSR/Chemistry - Iron, Solid Solution Jul/Aug 48
(Contd)

Submitted 15 Nov 1947.

8/49T10

C.A.

Rate of isothermal transformation of austenite as affected by composition in the system iron-carbon. I. I. Kornilov and A. A. Asovskaya. Izv. Akad. Nauk S.S.R. 10, No. 4, 85-95(1948).—It was observed that the rate of transformation of a system is closely connected with its compn., namely the max. rate of transformation coincides with stoichiometric compn., and the farther away from such compn., the longer it takes to attain equil. upon transformation. This investigation dealt with the transformation austenite \rightarrow ferrite + cementite, as affected by the C content. The Fe-C alloys studied contained only negligible admixts. of Mn, Si, S, and P. The C content varied from 0.18 to 0.94%. The alloys were heated for 30 min. at temps. 100° above the complete change to austenite, quenched in a Pb bath and the time for complete transformation was studied at 715 and 700°, and at 50° intervals down to 200°. The fastest transformation was at a C content of 0.18%. The time required for complete transformation increased with the C content up to 0.81% which is a eutectic and at 0.94% of C decreased again. The factors which detd. the rate of transformation were the concn. of the solid soln. and the nature of the new phase. As the concn. of the solid soln. increased, the rate of transformation decreased while the appearance of a new phase, cementite, hastened transformation. The min. rate coincided with the eutectic. Deviation from this was observed only when intermediate products such as martensite, troostite, etc., were formed.

M. Hoseh

C. 4.

5

Oxidation of solid solutions of chromium and aluminum in iron. I. I. Kurnikov. Izvest. Sektora Fiz.-Khim. Anal., Inst. Obshchel i Neorg. Khim., Akad. Nauk S.S.R., 16, No. 4, 122-9(1948).—In high temp. Al-Cr-Fe alloys the element most susceptible to oxidation is Al. At the surface of the ternary alloy Al oxidizes and the oxide gradually flakes off. The surface becomes impoverished in Al and therefore the alloy becomes thermodynamically unstable. This causes diffusion of Al atoms from the core toward the periphery. This process was studied on cylindrical specimens contg. Cr 27 and Al 5.8% at 1200° for 100 and 500 hrs. In both cases, there was a migration of Al from the center toward the periphery. The depth of the layer (from the periphery toward the center) where a diminution in the concn. of Al was observed after 100 hrs. was 2-2.5 mm, and after 500 hrs. 3-4 mm. The rate at which the concn. of Al decreased as affected by its original concn. in the Al alloy was studied on specimens contg. 1.5-9.5% Al, at 1200°, for up to 1000 hrs. The loss of Al was detd. by changes in resistivity, loss of wt., and chem. detn. of total Al. The relatively greatest changes, i.e. the highest rate of oxidation of Al was observed in alloys with the lowest Al content. Thus, an alloy contg. 1.5% Al lost during 1000 hrs. at 1200° 60% of it, while an alloy contg. 7.5 and 9.5% Al lost only 5-6%.

MP

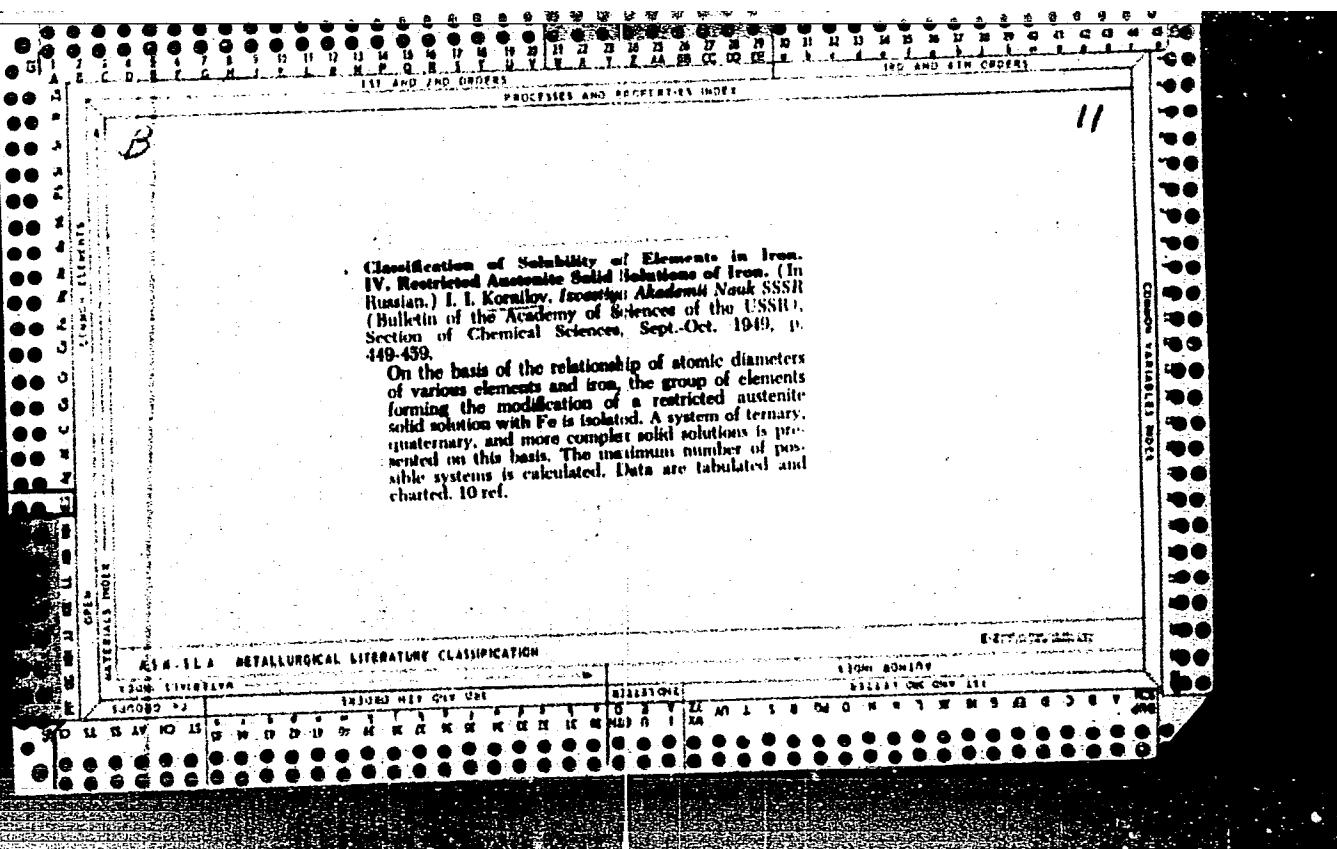
Properties of Alloys - 2

1954, III, 519; see *M.A.*, 2, 262; and Nekludov and Schamray, *Z. sov. Chem.*, 1955, 29(2), 348; *M.A.*, 8, 577).—R. N. H. "Magnesium-Manganese-Alloys of the System Magnesium-Aluminum-Manganese," N. V. Apov, L. I. Kurnikov, and A. N. Khlapov (*Izdat. Sots. Vuz. Khim. Akad.*, 1948, 18, (4), 130-143; *C. Abs.*, 1951, 65, 521).—[In Russian]. The purpose of the investigation was to determine the limit of solubility of Al and Mn when present together in solid Mg, to determine the boundaries of phases adjacent to the ternary solid soln., and to study the aging properties and corrosion-resistance of the alloys. The work was carried out on Mg alloys with up to 6% Al and up to 10% Mn. At the beginning of crystallization in the Mg region there separated first the α -phase, which is a ternary solid soln. having the crystal lattice of Mg. A Mn-rich phase separated next, and is referred to as X, the compn. of which was not determined. Next came γ , which is a solid soln. having a crystal lattice corresponding to Al_2Mg_3 , and a phase having the crystal lattice of Mn. In the presence of Al, the solubility of Mn in Mg at 450° C. rose from 0.3% to 1.25-1.5% and in slowly cooled alloy from 0 to 0.5-0.8%. The hardness of the alloys increased considerably with the Al content; lowering the Mn content did not appreciably affect the hardness. Alloys within the field of ternary solid soln. contg. Al 10-14 and Mn 0.2-0.8% could be aged artificially at 160°, 175°, and 200° C., and attained a max. hardness of 90-100 Brinell. At 100° C. the alloys aged very slowly and the hardness changed insignificantly. The preferred compns. for these alloys are: Al 10-13 and Mn 0.2-0.6%; the most corrosion-resistant alloys contained Al 2-7 and Mn 0.05-1.5%.

REMARKS. The method of aging of Mg-Al-Mn alloys (*Revue de Chimique*, 1950 (*C.A.* 32, 6728)) is proposed for its detn., because the method gives the most satisfactory results.
Emanuel Merlinger

1. Isothermal Ageing

Isothermal Transformation of Supersaturated Solid Solutions of Aluminum and Magnesium in Magnesium. I. I. Kurnikov and A. N. Khlapova (Izv. Akad. Nauk, Fiz. Khim., 1967, 198, 16, (4), 144-160; C. A., 1968, 68, 321). [In Russian]. The process of transformation was studied in alloys contg. Al 2-14.80 and Mn 0.10-1.15% at 100'-350' C. The alloys fall within the field of supersaturated ternary solid soln. Specimens were kept for 3 days sealed in evacuated tubes at 430' C. and were then transferred to a furnace maintained at the requisite temp. where they were kept for a definite time, after which they were water-quenched. At 330' and 300' C. the precipitated phase appeared in the form of large shiny particles throughout the entire field of the solid soln. There was no change in hardness. At 230'-150' C. the precipitated phase was pearlite; the precip. started along grain boundaries. Decompos. of the solid soln. at this temp. was accompanied by a considerable increase in hardness. At 100' C. no noticeable change was observed in the microstructure or hardness. The rate of transformation increased with the Al and Mn content. In consequence of the isothermal transformation the same hardness was attained as upon ordinary ageing, though in less time.



M

11-2

*Centrifugal Method for Determining the Strength of Metals and Alloys at High Temperatures. I. I. Kurnikov (Zarad. Lab., 1949, 18, (1), 76-82).--[In Russian]. Small round test-bars, with or without additional weights, are clamped to a rotor spinning at a const. regulatable speed in a furnace at a const. controlled temp. in the range room temp. to 1200° C. The relative strength of samples is proportional to the time necessary to attain the same or the max. state of deformation. Bending deformation continues indefinitely. The method can be used to choose quickly alloys with most suitable properties for a particular purpose and also to determine resistance to oxidation at high temp.; the test conditions correspond closely to the working conditions of alloys. The binary aluminium-magnesium alloys show greatest bending strength at 5% magnesium at 300° C.; the ternary iron-nickel-chromium system, tested for ratios of Fe : Ni = 3 : 1, shows greatest bending strength at 770° C. at ~25% chromium.—T. O. L.

Dec. 1960

KORNILOV, I.I.

New method for testing bending strength of metallic systems at
high temperatures. Izv. Sekt. fiz. khim. anal. 18:72-82 '49.
(MIRA 11:4)
I. Institut obshchey i neorganicheskoy khimii im. N.S. Kurnakova
AN SSSR.
(Metals—Testing) (Metals at high temperatures)

KORNILOV, I.I.; AZOVSKAYA, A.A.

Bending strength of aluminum - magnesium alloys at 300°C. Izv. Sekt.
fiz. khim. anal. 18:83-85 '49. (MIRA 11:4)

1. Institut obshchey i neorganicheskoy khimii im. N.S. Kurnakova
AN SSSR.
(Aluminum-magnesium alloys—Testing)

PA 66/49T40

USSR/Metals - Strength Aug 49

Alloys, High Temperature

"Application of Centrifugal Forces to the Study
of the Strength of Metallic Systems," I. I.
Kornilov, Inst of Gen and Inorg Chem, Imeni
N. S. Kurnakov, Acad Sci USSR, 3 pp

"Dok Ak Nauk SSSR" Vol LIVII, No 5

In 1945, revealed possibility and method of applying centrifugal forces to simplify method of testing the strength of metals, as existing methods proved unsatisfactory in handling test specimens at various temperature ranges. The never method must permit the comparative testing

66/49T40

USSR/Metals - Strength (Contd)

Aug 49

or many small samples at various temperatures at the same time, if high-temperature alloys are to be exploited. Present is a study of the necessary qualifications of an ultracentrifuge for testing alloys and metals, such as compactness, resistance to high temperatures (900°, 1,000°), high speeds (100,000 rev/min), etc. Diagram shows the arrangement of electric heating "oven" and centrifuge in the "oven," with motor and panel wiring scheme.

66/49T40

*M**2***"Theory of the High-Temperature Strength of Metallic Solid Solutions.**

J. I. Kornilov (*Doklady Akad. Nauk S.S.R.R.*, 1949, **67**, (6), 1037-1040; *C. A.*, 1950, **44**, 4844).—[In Russian]. A suggested measure of high-temp. strength is the time required for a specimen to creep or bend a predetermined amount in a centrifugal testing machine. By this means data were obtained for alloys of the binary systems: aluminium-magnesium at 200°, 250°, and 300° C.; copper-nickel at 400° C.; nickel-chromium at 800° C.; iron-chromium at 850° C.; on the 5% aluminium section of the iron-chromium-aluminium system at 800° and 1000° C.; on the 25% nickel, 75% iron section of the iron-chromium-nickel system; also on the 50% nickel, 50% iron section,

and on the 75% nickel, 25% iron section, all at 800° C.; on the quinary systems made up of 20% chromium, 30% iron, 40% nickel, and 10% manganese and 0-9% titanium, or 0-4% tungsten, or 0-15% niobium, all at 800° C. The high-temp. strength of a solid solution is higher than that of a pure metal and increases with increasing solute content. The high-temp. strength decreases when a second phase is produced by further addition of the solute. The concept "chemical hardening" by a solute atom is suggested in analogy with work-hardening.

27 May 1987

(A)

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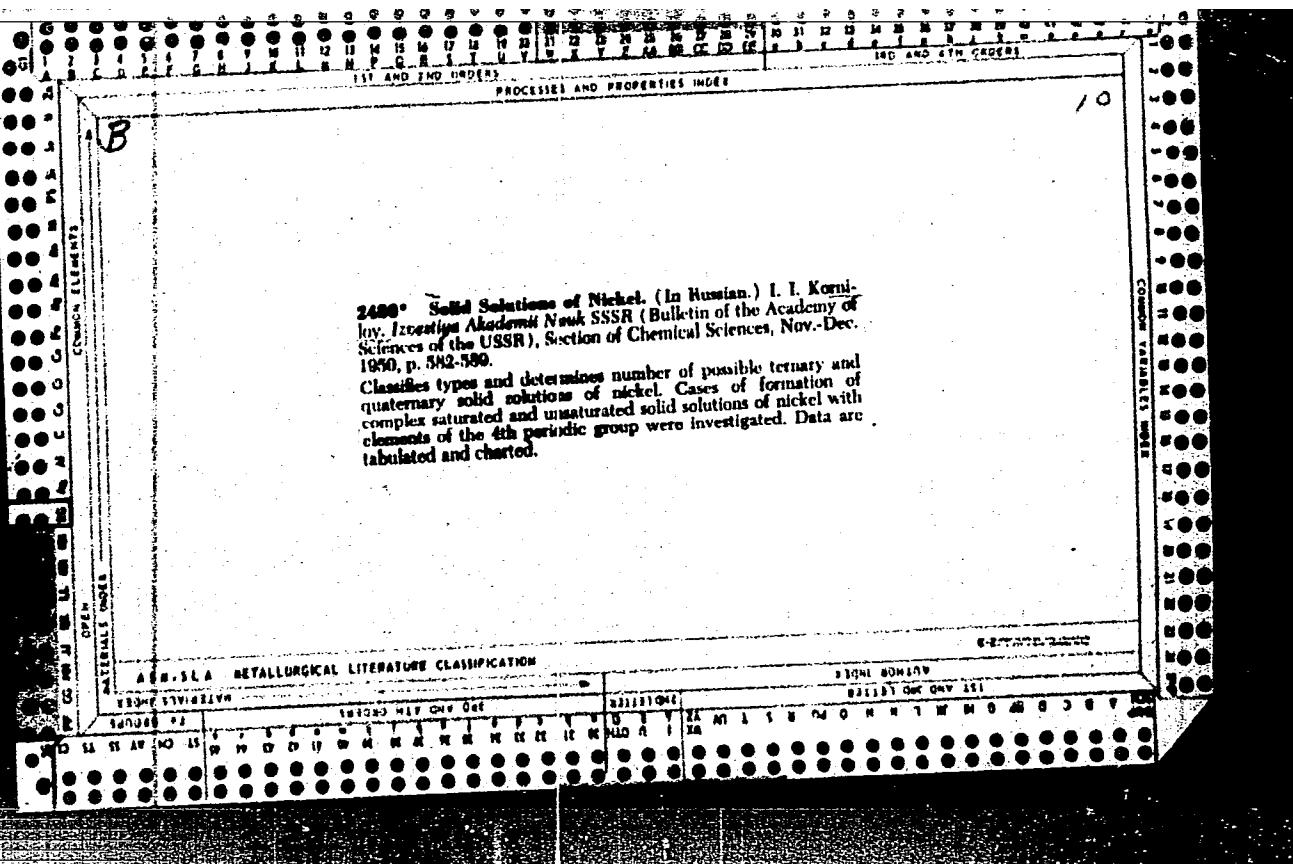
Study of the transformation of the α -solid solution in the iron-chromium system by the method of transformation velocity. I. I. Kurnikov and V. S. Mikhnev (N. S. Kurnakov Inst., Acad. Sci., U.S.S.R.), Doklady Akad. Nauk S.S.R. 58, 627-630 (1940).—An exptl. study was made of Fe alloys contg. from 40.48 to 54.70 at. % Cr. The time for 50% transformation of the solid soln. at 800° was detd. by a magnetometer and was found to have minima of 21 hrs. at 42.44 Cr, 33 hrs. at 46.44 Cr, and 62 hrs. at 49.57 at. % Cr. Between and beyond these compns. the half-time rose to about 1600 hrs. These data show the existence of three one-phase regions, β , θ , and ϵ , resp., with intervening eutectoid reactions involving $\beta + \theta$ and $\theta + \epsilon$. The eutectoid decompsn. did not go to completion in the 1925 hrs. of the expts. The curve of Curie temp. vs. compn. was continuous in the compn. ranges beyond and between the 3 one-phase regions.
A. G. Guy

*c A**5*

Solubilities of elements of the periodic system in nickel.
I. I. Kapitonov (N. B. Karacharov Inst. Gen. and Inorg. Chem., Acad. Sci. U.S.S.R., Moscow), *Izvest. Akad. Nauk S.S.R., Otdel. Khim. Nauk* 1960, 475-84.—Analysis of literature data shows that the rule of formation of solid soln. based on the comparability of the at. radii of the solvent and the solute is applicable to solid solns. in Ni. However, Ni has a somewhat greater tendency to form solid solns. than Fe, namely, it forms uninterrupted series of solid solns. up to an 11% difference in the at. radii (as against up to 8-9% in the case of Fe), and partial (limited) solid solns. up to 17-18% difference (as against up to 18-19% in the case of Fe). Plots of the solubilities in Ni by groups and periods of the periodic system permit predictions about the formation or the absence of solid solns. in Ni. Thus, uninterrupted solid solns. in Ni can be expected for Rh and Ir, and the existence of an uninterrupted solid soln. in the system Ni- γ -Mn is confirmed. Limited soln. in Ni can be expected for Ru, Os, and Re, on account of the differences of the crystal lattices of these elements and of Ni, and for P and U, on account of the differences of the at. radii (10 and 12.8%, resp.). Above all, or only insignificant solid soln. in Ni can be predicted, on account of the large difference of the at. radii (over 30%), for the Hf, Th, Sc, all elements of the 1st main group, and of the 2nd main group, with the exception of Be. Deviations from the solv. rule are found in the subgroups, e.g. Ag forms no solid solns. with Ni despite the favorable size factor, whereas Cu and Zn do form solid solns. despite an 18-20% difference in at. radii. Solubility in other elements of the VIIIth group, Co, Pt, and the Pt-series metals, can be inferred by analogy with Ni.

N. Tchou

1951



KORNILOV, I. I.

PA 160T75

USSR/Metals - Alloy Systems
Bismuth Compounds

May 50

"New Method for Studying Alloys by Samples of Variable Composition," I. I. Kornilov, N. V. V'yal', Inst of Gen and Inorg Chem, Acad Sci USSR, 3 pp

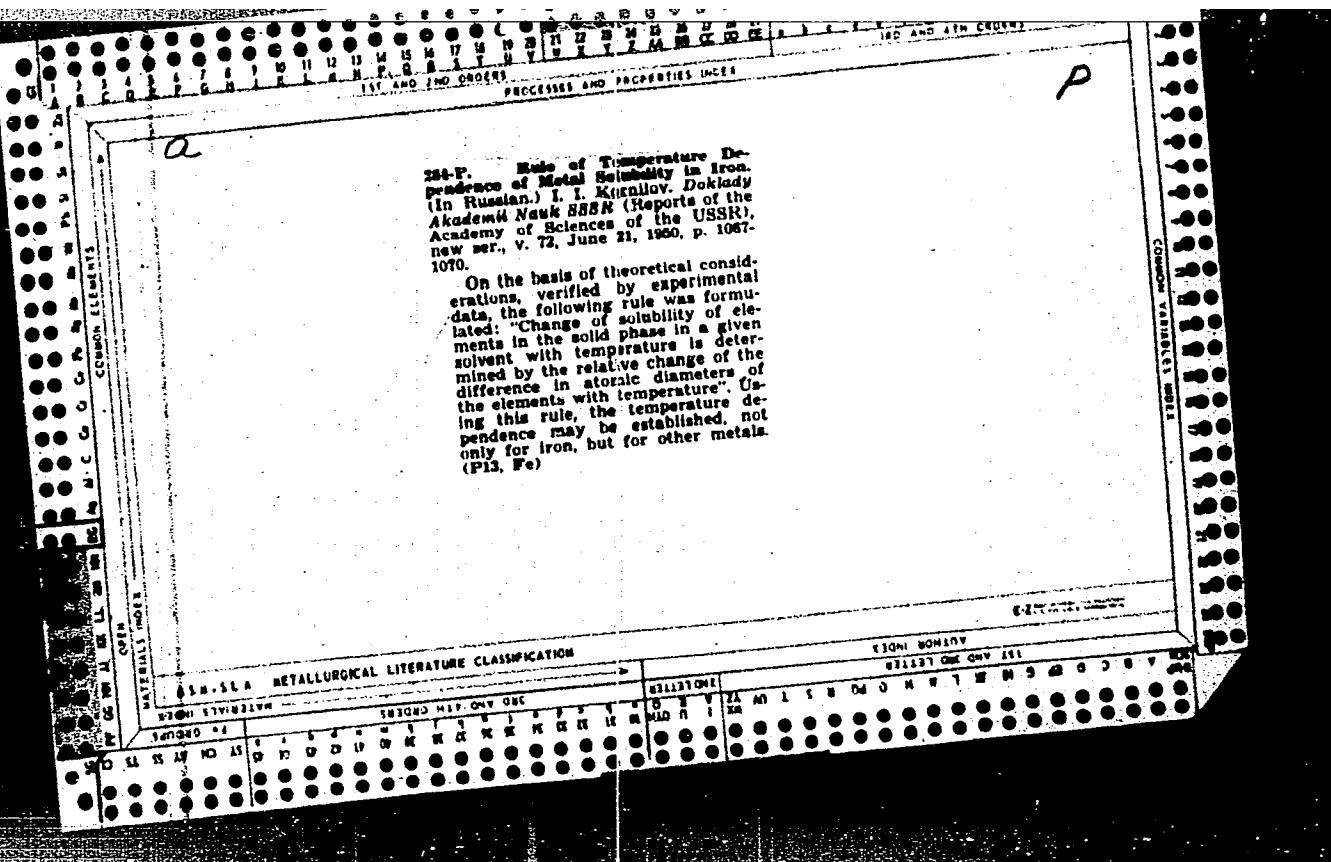
"Zavod Lab" Vol XVI, No 5

Offers method based on separating compounds of metal systems under action of centrifugal force in process of crystallization. Describes equipment and procedure for obtaining specimen of variable composition using alloy of bismuth with 10% cadmium. Method may be applied only for separating metals of different specific weights.

160T75

KORNILOV, I-I.

Time factor in physicochemical analysis. "I. I. Kornilov
Izdat. Sekcii fiz.-khim. anal., Akad. Nauk SSSR, 20
24-30 (1953).—Chem. reactions of Cu take place in 3×10^{-1} sec., the half period of ThC, but some transformations
in the solid state, e.g., silicates, take place within geologic
ages. The extremes are irrelevant in phys.-chem. analysis;
measurable rates of reaction are the important factors.
In phys.-chem. analysis the time factor is considered from
the point of view: (1) time required for a system to attain
equil. and the various stages of this system during this in-
terval; (2) effect of compn. on the time of transformation
within the system; (3) changes in compn. and properties of
a nonequil. system with time." M. Roseh



CA

Continuous solid solutions of transition elements. I. A.
Kapoor, Dabholkar, Ahad, Naik, S.S.I.R., 79, 466-7
(1980).—The radius ratio correlations between formation that
were found to hold for Fe-based alloys were examined to hold
also for all transition elements. Data from the literature
were available on 18 out of the 23 possible binary systems of
face-centered cubic metals, and all of these showed complete
solid solution. Data on 5 out of 18 body-centered cubic
systems gave the same result. No data were found
for systems involving two hexagonal metals. A. G. Guy

Review - B-77406, 21 Jul 54

Method of Representation of Quinary and the More Complex
Metallic Systems. I. I. Kornilov (*Doklady Akad. Nauk
SSSR*, 1961, 51 (2), 1961-1964). [In Russian]. A definite
chem. compn. of a binary (or more complex) solid soln. is
taken as origin, and addn. of the remaining three components
are represented on the x, y, and z co-ordinate axes, to give a
tetrahedral figure denoting an isolated region of the quinary
(or more complex) system. Parts of hypothetical Fe-Cr-Ni-
A-B and Fe-Cr-Ni-A-B-C systems are considered as
examples.—G. V. E. T.

KORNILOV, I. I.

SSSR/Chemistry - Metals

Dec 51

"Solid Solutions of Metal Compounds," I. I.
Kornilov

"Dok Ak Nauk SSSR" Vol LXXXI, No 4, pp 597-600

Shows on the basis of exptl material that solid solns of metal compds can be formed under the following conditions: (1) from metal compds of an ordered structure, (2) from metal compds of a const compn of Dalton's type, (3) from metal compds of a variable compn of Bertolet's type, and (4) from metal compds of both Dalton and Bertolet's type.

202T22

KÖRNILOV, I. I.

USSR/Academy of Sciences Chemistry - Electrochemistry

Jun 52

"Meeting of the Department of Chemical Sciences"

Vest Ak Nauk SSSR, No 6, p 112-115

At a session of the Dept Chem Sci concerned with the problem of electrochemistry, 4 reports were read, namely: "Reactions of Electrical Reduction and the Zero Points of Metals" by Acad A. N. Frumkin; "Diffusion Kinetics" by V. G. Levich; "Crystalllochemistry of Complex Thiocyanates" by O. S. Zhdanov; and "Metallic Compounds" by I. I. Kornilov.

PA 251772

BTR

1304 Solid Solutions: Classification of the Solubilities of Elements in Iron. Part II and III. L. I. Kornilov. Iron & Steel, v. 23, Jun. 1952, p. 25-30. (Translated from Izvestia Akademii Nauk SSSR)

In Part II a classification of solid solutions higher than binary involving iron is presented, based on the atomic diameters of the elements which form continuous (binary) solid solutions with iron and among themselves. Corresponding to the two modifications of iron (α and γ), two classes of continuous solid

solutions are considered: ferritic and austenitic. In Part III, from the relation of the atomic diameters of the elements and of iron, a group of elements with a difference of atomic diameters of 8-15% which form binary limited solid solutions with iron is isolated. A systematization of ternary, quaternary, and higher limited solid solutions of ferrite is given on the basis of these elements, and the number of possible systems is calculated. 27 ref.

KORNILOV, I. I.

"Scientific Sessions, Conferences, and Meetings - Meeting on the Theory of Metal Alloys," N. M. Abrikosov, Dr. Chem Sci., Vest Ak Nauk, No 8, p. 112, Aug 52.

At a meeting at the Inst of General and Inorg Chemistry imeni N. S. Kurnakov, Acad. Sci USSR, concerning metal alloys, N. V. Ageyev, Corr. Mbr. Acad. Sci USSR, presented a ~~MAX~~ report "Periodic Law of D. I. Mendeleyev - Basis of the Science of Metal Alloys." Also read were reports S. T. Konobeyevskiy, Corr. Mbr. Acad. Sci. USSR, on the "Nature of Combinations in Metals," and by Prof. I. I. Kornilov, on "Metal Chemistry and Some of its Problems." Plans were discussed for publication of a monograph and reference book on metal alloys.

252T47

KORNILOV, I. I.

Alloys

Development of N. S. Kurnakov's theories on the chemistry of metallic alloys. Usp.khim. 21, No. 9, 1952.

9. Monthly List of Russian Accessions, Library of Congress, December ¹⁹⁵² /1953. Unclassified.

USSR

Investigation of the diagram "composition-temperature-strength" of the quaternary system iron-chromium-nickel-manganese. I. I. Kornilov and K. A. Osipov. Bull. Acad. Sci. U.S.S.R., Div. Chem. Sci. 1953, 357-364 (Engl. translation). See C.A. 48, 133924.

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KORNILOV, I. I.

USSR/Metallurgy - Alloys, Heat Resistance

1 Oct 52

"Basic Types of Composition-Heat Resistance Diagrams of Metal Systems," I. I.
Kornilov
DAN SSSR, Vol 86, No 4, pp 721-724

States that numerous exptl data have been accumulated in past 6-7 years by using centrifugal method for investigating heat resistance of alloys; suggests 3 types of compn vs heat resistance diagrams of metal systems consisting of: (1) continuous solid solns with or without formation of compds from them; (2) limited solid solns with considerable concn range and solv varying with temp.; and (3) very limited solid solns or no solns at all. Presented by Acad G.G. Urazov 7 Aug 52.

(CA 48 no. 2:527 '54)

Source #264T49

KORNILOV, I. I.

PA 240T77

USSR/Metallurgy

- Aluminum-Magnesium

Heat Resistance Dec 52

"Effect of Temperature on the Heat Resistance of the Alloys of the Aluminum-Magnesium System," I. I. Kornilov and L. I. Pryakhina, Inst of General and Inorganic Chem imeni N. S. Kurnakov, Acad Sci USSR

"IMM SSSR" Vol 87, No 6, pp 971-974

Constructs for the first time compn vs heat resistance diagrams for alloys of Al-Mg system and, analyzing them, explains discrepancy in exptl data of various investigators. Some data show

240T77

max heat resistance in region of unsaturated solid solns, while data of other investigators place this max in region of complete satn. Submitted by Acad G. G. Urazov 20 Oct 52. Submitted

240T77

"APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R000824720006-2

USSR .

Solubility of chemical elements in chromium. I. I.

Kerzhov. Bull. Acad. Sci. U.S.S.R., Div. Chem. Sci.
1951, 871-7 (Engl. translation).—See C.A. 45, 78774.

H. L. H.

RE-
SAW

APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R000824720006-2"

KORNIL'YEV, I. I.

Journal of Applied Chemistry
June 1954
Industrial Inorganic Chemistry

(2)
Composition-hot strength diagram for alloys in the quaternary system, iron-chromium-nickel-manganese. I. I. Kornilov and K. A. Osipov (*Izvesia*, 1953, No. 3, 429-439). The electrical conductivity and hardness when quenched from 800° to room temp., and the resistance to plastic deformation (measured as the deflection on short rods after centrifugal loading for a definite time) at 600° ("hot strength"), are measured for various alloys in the system. The hot strength increases with the Cr content in the γ solid solution region, but sharply decreases with it above saturation or in the γ+α region, where the hardness at room temp. increases with the Cr content. Changes in Mn content exert little effect on the mechanical properties, and Mn can be largely replaced by Ni.

R. C. MURRAY

KORNILOV, I. I.

The Committee on Stalin Prizes (of the Council of Ministers USSR) in the fields of science and inventions announces that the following scientific works, popular scientific books, and textbooks have been submitted for competition for Stalin Prizes for the years 1952 and 1953. (Sovetskaya Kultura, Moscow, No. 2240, 20 Feb - 3 Apr 1954)

<u>Name</u>	<u>Title of Work</u>	<u>Nominated by</u>
Kornilov, I. I.	"Solid Solutions and Compounds of Metals"	Institute of Metallurgy imeni A.A. Baykov, Academy of Sciences USSR

SC: W-30604, 7 July 1954

KORNILLOV, I.I.

USSR/ Chemistry - Physical chemistry

Card 1/1 : Pub. 40 - 5/22

Authors : Kornillov, I. I.

Title : Metallic compounds

Periodical : Izv. AN SSSR. Otd. khim. nauk 5, 795-804, Sep-Oct 1953

Abstract : The differences in the properties of metallic and ion compounds are explained. The atoms of opposite sign in metallic compounds are bound with each other in the crystalline lattice, preferably by a metallic bond, which in contrast to metallic solid solutions fixes the constant stoichiometric ratio of the atoms in the compound. The laws governing the formation of metallic solutions and metallic compounds are especially important for the determination of the nature of reaction of metals and prognosis of structural diagrams in non-investigated systems. Eighteen references: 17-USSR and 1-USA (1911-1952). Table; graphs.

Institution : Acad. of Sc. USSR, The N. S. Kurnakov Institute of Gen. and Inorg. Chemistry

Submitted : January 1, 1953

USSR/Metallurgy - Alloys

Nov/Dec 53

The Solubility of Chemical Elements in Chromium.
I.I. Kornilov, Inst. Gen. and Inorg. Chem. im N.S.
Marakov, Acad. Sci USSR.

Iz Ak Nauk SSSR, OGDN, No 6, pp 980-987

Established relationships pertaining to the solubility of elements in the form of solid solns in Cr. Concludes that the regularities established will aid in investigating solid solns based on Mb and W. Points out the significance of this work for the technology of heat-resistant alloys.

273r68

Translation B-77406, 21 Jul 54

"APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R000824720006-2

KORNILOV, I. I. and MIKHEYEV, V. A.

"Constitution Diagrams of Metallic Systems Based on Chromium," Uspekhi
Khimii 22 (1953) pp 87/98.

B-77406, 21 Jul 54

APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R000824720006-2"

KORNILOV, I.I.; MINTS, R.S.

Structural diagram of the system Cr -- NiAl. Izv.Sekt.fiz.-khim.anal.
22:111-116 '53. (MLRA 7:5)

1. Institut obshchey i neorganicheskoy khimii im. N.S.Kurnakova
Akademii nauk SSSR. (Chromium-nickel-aluminum alloys)

KORNILOV, I. I.

Solid State Physics, Thermodynamics (4898)

Izv. Sektora Fiz.-Khim. Analiza (Inst. Obshch. i Neorgan. Khimii A. N. SSSR),
No 22, 1953, pp 117-121

Kornilov, I. I., and Nikolayenko, G. M.

Phase Diagram of the System Nickel-Chromium-Manganese

Microstructural method using 12 cross sections was used to investigate phase diagram at room temperature of Ni-Cr-Mn. Solubility of Cr in Ni was found 35%, Mn in Ni about 36%, and maximum of joint Cr and Mn solubility was 24% Cr + 24% Mn.

So: Moscow, Referativnyy, Zhurnal -- Fizika, No 5, 1954 W-31059

Diagram of state of the system nickel-tantalum. I. I.
Korubov and B. N. Petrenko. *Transl. Sessiora Fiz. Akademii
Nauk SSSR*, 27, 110-17 (1933).—The studied
alloys contained up to 60.04% Ta. At a Ta content up to
36%, crystal. solid solns. of Ta in Ni were present. At
36-60%, Ta crystal. as Ni₄Ta and its solid solns. The max.
m.p., 1504°, was observed for an alloy contg. 50.7% Ta,
which is close to Ni₄Ta contg. 50.7% Ta and for which
Therkelsen (*C.A.*, 27, 4513) gives the m.p. as 1545°. On
either side of Ni₄Ta there is a eutectic. The 1st coincides
with 37.80% Ta and m. 1360°. The other eutectic was not
detd. Data in literature place it at 61% Ta and m. 1400°.
The solv. of Ta in Ni as function of temp. was detd. to be
37.8% at 1300°, 33% at 1300°, 30% at 1200°, 21% at
1100°, 14% at 1000°, and 7.5% at 800°. Hardness and
electroresistances increased with the Ta content. Analysis
of the extraneous phase showed it to be a solid soln. of Ni in
Ni₄Ta contg. 40.44% Ta. f. M. Hoach

USSR/Metallurgy - Nonferrous Alloys
Heat Resistance 1 Feb 53
"Composition Versus Heat Resistance of the
Ni-Al System," I. I. Kornilov, R. S. Mints,
S. D. Onopriyenko, Inst of General and Inorg Chem,
Acad Sci USSR
DAN SSSR, Vol 88, No 4, pp 683-685

Studies dependence of heat resistance on compn of
Ni-Al alloys up to 30% Al by wt. Establishes that
heat resistance of solid solns of Al in Ni increases
with increase in Al concn and reaches its max in
region of complete satn of solid solns. Alloy

corresponding to Ni₃Al is characterized by lowest
heat resistance; solid solns based on Ni₃Al, rich
with Ni or Al, have heat resistance higher than
that of Ni₃Al. States that diagram of compn vs
heat resistance permits detn of physicochem nature
and boundaries of phase areas on Ni-Al constitution
diagram. Presented by Acad G. G. Urazov 29 Nov 52.

PA 249T60

249T60

KORNILOV, I-I.

met 2

J. of the Inst. of Metals
Feb. 1951
Properties of Alloys

Separation of Nickel Tantalide, Ni₃Ta, from Alloys of the Binary System Nickel-Tantalum. I. I. Kornilov and E. N. Pel'cheva (*Doklady Akad. Nauk S.S.R.*, 1953, 91, (4), 841-842).—[In Russian]. By heating *in vacuo* at 1300° C. for 4 hr., at 1200° C. for 2 hr., at 1000° C. for 2 hr., and then slowly cooling to room temp., K. and P. produced a considerable coarsening of the Ni₃Ta phase (present as elongated crystals) in the two-phase alloy of Ni with 30-15% Ta. They found that 5% HCl contg. 2-3 drops HNO₃ was best for dissolving the Ni solid soln. without attacking the Ni₃Ta. With 0.2-0.5 g. alloy in a 100-ml. beaker, dissolution began only on warming, but then continued very slowly in the cold for 2-3 days, with occasional agitation. The residue was dried with alcohol and ether and observed microscopically. Greater amounts were prepared by electrolytic dissolution, using as anode a polished rod of the alloy 50 × 3 mm. dia. in a colloid bag, contred with relation to the tinplate beaker, 9 cm. high × 8 cm. wide, acting as cathode. The electrolyte was 0.75% alcoholic HCl + 20 g. citric acid + 5 g. NH₄Cl, and the o.d. 0.01 atm./cm.² (at greater o.d. there was anodic oxidation, so that the product contained oxide and salts). 0.5 g. powder was obtained in 1 hr. On analysis by dissolving in HF + HNO₃, removing HF by heating with H₂SO₄, precipitating Ta with NH₄OH in the presence of NH₄Cl, and weighing as Ta₂O₅, the powder was found to contain 49.44% Ta (cf. 50.71% for Ni₃Ta theoretically).—G. V. E. T.

Inst. Gen.-le Inorganic Chem. im. N. S. Kurnakov, AS USSR.

Kornilov, I. I.

✓ The compound NiAl. I. I. Kornilov and R. S. Mints.
Doklady Akad. Nauk SSSR, 88, 529-32 (1953); cf.
62 *C.A.* 49, 3600e.—The metallic compds. NiAl (I) and NiAl
(II) show min. resistivity and a max. temp. coeff. of re-
sistivity on corresponding compn.-property diagrams. I
shows a singular min. on the coeff. of linear expansion iso-
therm whereas II gives only a negligible effect. The coeff.
of linear expansion of I is considerably lower than for pure
Ni and a solid solz. of Al in Ni. I gives an identical singular
point on all known property-compn. diagrams including
heat resistance. Discrepancy in direction of the isotherm
of coeff. of linear expansion for annealed and quenched al-
loys leads to the possibility of transformation of I in the
solid state at temps. near 600°. V. N. Eddnaraki

(1)

KORNILOV, I.I.

B. T. R.
V. 3 No. 3
Mar. 1954
Metals- Metal-
lography, Trans-
formations, and
Structures

3937¹ Basic Types of Constitution Diagrams of Titanium
Base Binary Systems. (Russian.) I. I. Kornilov. *Doklady Akademii Nauk SSSR*, v. 91, no. 3, July 21, 1953, p. 549-552.
Position in the periodic system of Ti and its alloying elements
and similarity or differences of their chemical properties determine
characteristics of their interactions and consequently the
types of phase diagrams. Graphs. 16 ref.

Inst. Metallurgy. AS USSR

"APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R000824720006-2

KORNILOV, I. I.

"Creep of Solid Solutions and Compounds in Metallic Systems," a study presented at the Symposium and International Conference on Creep and Fracture of Metals at high Temperature, Teddington, England, 31 May to 2 Jun 1954.

S-3146, 30 Dec 54

APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R000824720006-2"

USSR/Chemistry Solubility

Card : 1/1

Authors : Kornilov, I. I.

Title : Solubility of chemical elements in titanium

Periodical : Izv. AN SSSR, Otd. Khim. Nauk., 3, 392 - 399, May - June 1954

Abstract : The analogous sequence existing between the solubility of chemical elements of the periodical system in titanium and the solubility of elements in other metals (iron, nickel, chromium, etc.) is discussed. The difference in chemical properties of elements and their effect on the formation of solid solutions or their absence in binary titanium systems, are explained. Metals of the V and VI groups analogous to titanium, which have small differences in atom diameters and isomorphic structure, but when combined with titanium are capable of yielding continuous solid solutions, are described. Thirty-eight references: 8 USSR, 3 German, 27 USA. Tables, graphs.

Institution : Acad. of Sc. USSR, The N. S. Kurnakov Inst. of Gen. and Inorg. Chem.

Submitted : July 9, 1953

KORNILOV, I. I.

"Titanium, Its Properties, Application and Methods of Preparation," Usp. Khim.,
No 5, pp 529-546, 1954

Translation M-422, 6 May 55

6

✓ *The Relation Between the Composition, Temperature,
and Strength of Aluminum-Magnesium Alloys. I. I. Kosyukov
and L. I. Pravkina. (Izv. Akad. Nauk S.S.R., 1954.)

USSR

[Tekhn. J. (9), 85-89].—[In Russian]. The influence of temp. upon the strength of Al-Mg alloys was studied between 20° and 400° C. in relation to the compn. in the range 0-12 wt.-% Mg. The specimens were subjected to bending tests, and for each temp. a different value of stress was chosen in order to produce slow deformation in the course of several tens or hundreds of hr. At 400° C. the max. strength was shown by pure Al; at lower temp. the region of alloys of high strength shifted gradually towards the alloys contg. more Mg, the max. becoming wider as the temp. was lowered. Thus, at 300° C., the alloys contg. 6-6 wt.-% Mg possessed the greatest strength; at 29° C., those contg. 4-12 wt.-% Mg. Above 300° C., the alloys which retained most strength were homogeneous solid soln. of Mg in Al. The max. strength at 300° C. corresponded to the max. solubility of Mg in Al, and below 200° C. to the alloys composed of two phases. This behaviour was explained by the fact that the solidus temp. of the homogeneous solid soln. is higher than the initial m.p. of the two-phase alloys.—S. K. L.

MG

(1)

Mg

KORNILOV, I.I.
USSR/Scientific Organization - Conferences

Card 1/1 Pub. 124 - 9/26

Authors : Kornilov, I. I., Dr. of Chem. Sc.

Title : Conference of creep and destruction of metals at high temperatures

Periodical : Vest. AN SSSR 12, 57-59, Dec 1954

Abstract : Minutes are presented of the conference held in London, England during May 31 - June 2, 1954, at which problems of creep and destruction of metals at high temperatures were discussed. The conference was called by the largest English Scientific Organization - National Physics Laboratory and was attended by metallurgical scientists from all Western Nations including the USA and Japan. The USSR was the only representative of East European Nations invited to the conference.

Institution : ...

Submitted : ...

KORNILOV, I.I.

AID P - 1111

Subject : USSR/Chemistry

Card 1/1 Pub. 119 - 1/7

Author : Kornilov, I. I. (Moscow)

Title : Titanium: properties, use and methods of production

Periodical : Usp. khim., 23, no. 5, 529-546, 1954

Abstract : Production and properties of metallic titanium are reviewed, based in the main on non-Russian literature. Ten diagrams, 4 tables, 37 references (8 Russian: 1941-1954).

Institution : None

Submitted : No date

*KORNILOV**200**67*

Melting Diagram of the System Nickel-Chromium-NiAl
I.I. Kornilov and Yu.S. Mintz *Doklady Akad. Nauk S.S.R.R.*,
1954, *M.*, (8), 1085-1088).—(In Russian). The melting
diagram of the ternary system Ni-Cr-NiAl was prepared,
starting with an investigation of the binary systems Ni-Cr,
Ni-NiAl, and Cr-NiAl by the method of thermal analysis
and microhardness determinations. The liquidus surface of the system
Ni-Cr-NiAl was then constructed with the aid of orthogonal
projections of the liquidus lines of sections of const. content
of 20, 30, 40, 50, and 60 wt.-% Cr; 20, 30, 40, 50, and 60
wt.-% Ni; 10, and 20 wt.-% NiAl upon the compn. triangle.
It consisted of four fields of primary crystallization corresponding
to the espn. of the following phases: (i) α solid soln. of Ni and
Al in Cr, (ii) β solid soln. of Ni and Cr in NiAl, (iii) γ solid
soln. of Cr and Al in Ni, and (iv) γ' solid soln. of Cr, Ni, and Al
in Ni₃Al. The lines of secondary crystallization and of phase struc-
ture and the behaviour under heat-treatment of several
Ni-Cr-NiAl alloys of intermediate compn. were also de-
termined. It was concluded that the peritectic reaction giving
rise to Ni₃Al takes place between the liquid and the
 β phase of NiAl (cf. Taylor and Flynn, *J. Inst. Metals*, 1952-
53, **81**, 481; *M.A.*, 20, 691) and not between the liquid and the
Ni γ solid soln. (cf. Alexander and Vaughan, *Ibid.*, 1937, **62**,
247; *M.A.*, 4, 614).—S. K. L.

Evaluation B-80678

KORNILOV, I. I.

3

*The Compound Ni₂Cr. I. I. Kornilov and R. H. Mints
[Doklady Akad. Nauk SSSR, 1954, 96, 73, 543-546].—
[In Russian]. Alloys of Ni contg. 0-35 at.-% Cr were ex-
amined, before and after annealing at different temp., by
metallographic and X-ray analysis and by dilatometric
and elect.-resistance data. (cf. Taylor and Hinton, J. Inst.
Metals, 1952-53, 81, 169; M.A., 20, 337). The sp. elect.
resistance of the specimen annealed at 460° C. was lower than
the resistance of the quenched specimens, the difference
increasing with the time of annealing. A sharp min on the
sp. elect. resistance/at.-% Cr curve corresponding to 24 at.-%
Cr indicated the formation of the Ni₂Cr compound. A
similar sharply defined min. was discovered on the linear
expansion coeff./at.-% Cr diagram. X-ray analysis showed a
decrease of the cell const. a after annealing; for the alloy
contg. 24 at.-% Cr, $a = 0.633$ and 3.624 Å for the quenched
and annealed specimens, resp.—S. K. L.

Evaluation B-80678

KORNILOV, I. I.

USSR/ Chemistry - Metallurgy

Card : 1/1

Authors : Kornilov, I. I. and Pylaeva, E. N.

Title : Study of the structural diagram of a system formed by metallic Ni₃Nb-Ni₃Ta compounds.

Periodical : Dokl. AN SSSR, 97, Ed. 3, 455 - 457, July 21, 1954

Abstract : The study and formation of a structural diagram, for a binary system formed by metallic Ni₃Nb and Ni₃Ta compounds, are discussed. The study of this system was carried out by methods of thermal analysis, microstructure, specific electrohardness, resistance and specific weight. Many fusions of this binary system were also subjected to x-ray analysis and the total results are described. Eight references: 6-USSR and 2-USA.
Graph, illustrations.

Institution : Acad. of Sc. USSR, The A. A. Baykov Institute of Metallurgy

Presented by : Academician I. P. Bardin, March 26, 1954

KORNILOV, I. I.

USSR/Chemistry - Metallic compounds

Card 1/2 Pub. 22 - 24/47

Authors : Kornilov, I. I., and Matveyeva, N. M.

Title : Constant solid solutions of metallic FeCr and FeV compounds

Periodical : Dok. AN SSSR 98/5, 787-790, Oct 11, 1954

Abstract : The existence of a continuous series of solid alpha solutions in the ternary Fe - Cr - V system at high temperatures and the formation of a continuous series of solid sigma solutions between FeCr and FeV compounds was confirmed by thermal analysis, hardness and micro-structural methods. The process and rate of formation of such solid sigma compounds, from solid alpha solutions, are explained. The temperatures leading to conversion of solid solutions of the sigma FeCr and FeV compounds into ternary solid solutions of alpha compounds, which constitute the ternary system of metals, were found to be of continuous nature and correspond to conversions of solid sigma solutions into

Dok. AN SSSR 98/5, 787-790, Oct 11, 1954

(Additional card)

Card 2/2

Abstract : solid solutions of alpha metals. Nine references: 8-USSR and 1-US (1936-1954). Graphs.

Institution: Acad. of Sc. USSR, The A. A. Baykov Metallurgical Institute

Presented by: Academician G. G. Urazov, May 22, 1954

USSR/Engineering - Metallography

FD-2240

Card 1/1 Pub 41-8/17

Author : Kornilov, I. I. and Kosmodem'yanskiy, V. V., Moscow

Title : Relationship between composition, temperature, and heat resistance. II.
Ternary system Nickel-Chromium-Titanium alloys

Periodical : Izv. AN SSSR, Otd. Tekh. Nauk 2, 20-97, Feb 1955

Abstract : Studies the relationship between composition, structure, and heat resistance of Ni-Cr-Ti ternary system alloys over a wide temperature range (500-1200°). Twenty different alloys were tested. The chromium content was constant at 20% while titanium content was varied from 0% to 10%. Titanium solubility was investigated at the following temperatures: 700°, 800°, 900°, 1000°, 1100°, and 1200°. Diagrams. Eight references, 7 USSR.

Institution:

Submitted : January 21, 1955

KORNILOV, I. I.
USSR/Engineering - Physical Metallurgy

FD-3227

Card 1/1 Pub. 41-8/22

Author : Kornilov, I. I. and Snetkov, A. Ya., Moscow

Title : Study of the Limited Solid Solutions of Nickel by the X-ray
Structural Method

Periodical : Izv. AN SSSR, Otd. Tekh. Nauk 7, 84-88, Jul 55

Abstract : Investigates the variation of value a (lattice spacing) in
relation to the content and relative atomic diameters of
alloying elements in binary and ternary nickel alloys. Con-
cludes that chromium, which differs little from nickel in its
atomic diameter, effects only a small distortion of the crystal
lattice of nickel. Three tables; two diagrams. Twelve references,
nine USSR.

Institution :

Submitted : 26 January 1955